

## **New Residential Development**

**52 Coldharbour Lane,  
Hayes, UB3 3EP.**

### **Noise Impact Assessment**

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Project Address:	52 Coldharbour Lane Hayes UB3 3EP
Project Reference:	104753

**Issue/Revision Record**

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## 1. INTRODUCTION

- 1.1 Acoustics Plus Ltd (APL) is an independent firm of multi-disciplinary acoustic engineers. APL is engaged by both private and public sector clients. APL is a registered member of The Association of Noise Consultants (ANC) and the author is a corporate member of The Institute of Acoustics (IOA).
- 1.2 APL has been instructed by Kamal Property Services Ltd to consider and advise upon the noise implications regarding the erection of three storey building (plus basement level) to provide a mixed use building comprising commercial Class E and Class F1 units and 9No. flats with associated refuse, parking and landscaping following demolition of the existing building.
- 1.3 It is understood that the Local Planning Authority (LPA) will require additional information, specifically in regard of noise. It is further understood that the noise matters are in connection with the proposed new residential accommodations proximity to nearby highways and commercial activities.
- 1.4 The object of this report is to determine environmental noise levels at the proposed site in accordance with Government planning policy. Outline comments regarding noise control measures are provided to demonstrate that the ingress of noise may be properly controlled.
- 1.5 The report will give due regard to the following documents:
  - a) *National Planning Policy Framework; February 2025 – Ministry of Housing, Communities & Local Government.*
  - b) *Noise Policy Statement for England (NPSE) March 2010 – Department for Environment, Food and Rural Affairs.*
  - c) *ProPG: Planning and Noise May 2017 Professional Practice Guidance on Planning and Noise.*
  - d) BS 8233:2014 “Sound insulation and noise reduction for buildings – Code of Practice”.
- 1.6 This report has been prepared by Acoustics Plus Limited (APL) with all reasonable skill, care, and diligence in accordance with generally accepted acoustic consultancy principles and taking account the services and terms agreed between APL and our client.
- 1.7 Any information provided by third-parties and referred to herein may not have been checked or verified by APL unless expressly stated otherwise. Certain statements made in the report are predictions based on reasonable assumptions and good industry practice.
- 1.8 Such statements involve risk and uncertainty which could cause measured and predicted results to differ materially. APL does therefore not guarantee or warrant any prediction contained in this report.

## 2. BASELINE SITUATION

2.1 The Application Site (the “site”) is located at 52 Coldharbour Lane, Hayes, UB3 3EP. A sitemap plan is shown in Diagram 1 below.



Diagram 1

2.2 The application proposes the erection of three storey building (plus basement level) with to provide a mixed use building comprising commercial Class E and Class F1 units and 9No. flats with associated refuse, parking and landscaping following demolition of the existing building.

2.3 The site and surrounding area are shown within the Figures appendix of this report.

### 3. NOISE CRITERIA

#### NATIONAL PLANNING POLICY FRAMEWORK

3.1 The National Planning Policy Framework (NPPF) was most recently updated in February 2025 and has replaced planning policy guidance which previously covered planning and pollution control and new development in England. The purpose of the planning system is to contribute to the achievement of sustainable development. There are three dimensions to sustainable development: economic, social and environmental. The environmental role is to contribute to protecting and enhancing our natural, built and historic environment; including making effective use of land, helping to improve biodiversity, using natural resources prudently, minimising waste and pollution, and mitigating and adapting to climate change, including moving to a low carbon economy.

3.2 One of the core planning principles is to contribute to conserving and enhancing the natural environment and reducing pollution. Planning policies and decisions should contribute to and enhance the natural and local environment by;

- *protecting and enhancing valued landscapes, sites of biodiversity or geological value and soils (in a manner commensurate with their statutory status or identified quality in the development plan).*
- *recognising the intrinsic character and beauty of the countryside, and the wider benefits from natural capital and ecosystem services – including the economic and other benefits of the best and most versatile agricultural land, and of trees and woodland.*
- *maintaining the character of the undeveloped coast, while improving public access to it where appropriate.*
- *minimising impacts on and providing net gains for biodiversity, including by establishing coherent ecological networks that are more resilient to current and future pressures and incorporating features which support priority or threatened species such as swifts, bats and hedgehogs.*
- *preventing new and existing development from contributing to, being put at unacceptable risk from, or being adversely affected by, unacceptable levels of soil, air, water or noise pollution or land instability. Development should, wherever possible, help to improve local environmental conditions such as air and water quality, taking into account relevant information such as river basin management plans; and*
- *remediating and mitigating despoiled, degraded, derelict, contaminated and unstable land, where appropriate.*

3.3 Paragraph 198 of the NPPF states Planning policies and decisions should also ensure that new development is appropriate for its location taking into account the likely effects (including cumulative effects) of pollution on health, living conditions and the natural environment, as well as the potential sensitivity of the site or the wider area to impacts that could arise from the development. In doing so they should:

- *mitigate and reduce to a minimum potential adverse impacts resulting from noise from new development – and avoid noise giving rise to significant adverse impacts on health and the quality of life;*
- *identify and protect tranquil areas which have remained relatively undisturbed by noise and are prized for their recreational and amenity value for this reason; and*
- *limit the impact of light pollution from artificial light on local amenity, intrinsically dark landscapes and nature conservation.*

3.4 Paragraph 187 of the NPPF states that:

*“Planning policies and decisions should contribute to and enhance the natural and local environment by.... e) preventing new and existing development from contributing to, being put at unacceptable risk from, or being adversely affected by, unacceptable levels of soil, air, water or noise pollution or land instability.”*

3.5 The Government's long-term policy aims relating to noise are contained in the Noise Policy Statement for England (referred to as NPSE). Stated aims of the NPSE are:

*“Through the effective management and control of environmental, neighbour and neighbourhood noise within the context of Government policy of sustainable development:*

- *Avoid significant adverse impacts on health and quality of life;*
- *Mitigate and minimise adverse impacts on health and quality of life; and*
- *Where possible, contribute to the improvement of health and quality of life.*

3.6 The Professional Practice Guidance on Planning and Noise (ProPG) has been produced to provide practitioners with guidance on a recommended approach to the management of noise within the planning system in England. The recommended ProPG internal noise level guidelines are described in the table below. These guidelines reflect and extend current practice contained in BS8233:2014 (Sound Insulation and Noise Reduction for Buildings – Code of Practice). For clarity, blue italic font is used to highlight additions to the guidance contained in Table 4 of BS8233:2014. The dB values provided in the table for different activities are target levels. The table plus supporting notes are referred to as ProPG internal noise level guidelines.

Activity	Location	07:00-23:00hrs	23:00-07:00hrs
Resting	Living room	35dB L <sub>Aeq,16hr</sub>	-
Dining	Dining room/area	40dB L <sub>Aeq,16hr</sub>	-
Sleeping (daytime resting)	Bedroom	35dB L <sub>Aeq,16hr</sub>	30dB L <sub>Aeq,8hr</sub> 45dB L <sub>Amax,F</sub>

Table 1

**NOTE 1** The Table provides recommended *internal LAeq target* levels for overall noise in the design of a building. These are the sum total of structure-borne and airborne noise sources. Ground-borne noise is assessed separately and is not included as part of these targets, as human response to ground-borne noise varies with many factors such as level, character, timing, occupant expectation and sensitivity.

**NOTE 2** The *internal LAeq target* levels shown in the Table are based on the existing guidelines issued by the WHO and assume normal diurnal fluctuations in external noise. In cases where local conditions do not follow a typical diurnal pattern, for example on a road serving a port with high levels of traffic at certain times of the night, an appropriate alternative period, e.g. 1 hour, may be used, but the level should be selected to ensure consistency with the *internal LAeq target* levels recommended in the Table.

**NOTE 3** These *internal LAeq target* levels are based on annual average data and do not have to be achieved in all circumstances. For example, it is normal to exclude occasional events, such as fireworks night or New Year's Eve.

**NOTE 4** Regular individual noise events (for example, scheduled aircraft or passing trains) can cause sleep disturbance. A guideline value may be set in terms of SEL or L<sub>Amax,F</sub>, depending on the character and number of events per night. Sporadic noise events could require separate values. *In most circumstances in noise sensitive rooms at night (e.g. bedrooms) good acoustic design can be used so that individual noise events do not normally exceed 45dB L<sub>Amax,F</sub> more than 10 times a night. However, where it is not reasonably practicable to achieve this guideline then the judgement of acceptability will depend not only on the maximum noise levels but also on factors such as the source, number, distribution, predictability and regularity of noise events (see Appendix A).*

**NOTE 5** Designing the site layout and the dwellings so that the *internal target levels* can be achieved with open windows in as many properties as possible demonstrates good acoustic design. Where it is not possible to meet *internal target levels* with windows open, internal noise levels can be assessed with windows closed, however any façade openings used to provide whole dwelling ventilation (e.g. trickle ventilators) should be assessed in the "open" position and, in this scenario, the *internal LAeq target levels* should not normally be exceeded, subject to the further advice in Note 7.

**NOTE 6** Attention is drawn to the requirements of the Building Regulations.

**NOTE 7** Where development is considered necessary or desirable, despite external noise levels above WHO guidelines, the *internal LAeq target levels* may be relaxed by up to 5 dB and reasonable internal conditions still achieved. *The more often internal LAeq levels start to exceed the internal LAeq target levels by more than 5 dB, the more that most people are likely to regard them as "unreasonable". Where such exceedances are predicted, applicants should be required to show how the relevant number of rooms affected has been kept to a minimum. Once internal LAeq levels exceed the target levels by more than 10 dB, they are highly likely to be regarded as "unacceptable" by most people, particularly if such levels occur more than occasionally. Every effort should be made to avoid relevant rooms experiencing "unacceptable" noise levels at all and where such levels are likely to occur frequently, the development should be prevented in its proposed form (see Section 3.D).*

## COMMERCIAL NOISE INGRESS

3.7 This assessment considered the principals of contained within Policy D 14 Noise of The London Plan 2021:

### Policy D14 Noise

A In order to reduce, manage and mitigate noise to improve health and quality of life, residential and other non-aviation development proposals should manage noise by:

- 1) avoiding significant adverse noise impacts on health and quality of life
- 2) reflecting the Agent of Change principle as set out in Policy D13 Agent of Change
- 3) mitigating and minimising the existing and potential adverse impacts of noise on, from, within, as a result of, or in the vicinity of new development without placing unreasonable restrictions on existing noise-generating uses
- 4) improving and enhancing the acoustic environment and promoting appropriate soundscapes (including Quiet Areas and spaces of relative tranquillity)

3.8 In demonstrating that the development proposals are suitably mitigated and that the commercial uses proposed to be located below the site would adversely impact the residential dwellings above, guidance regarding the noise levels not to be exceeded from commercial noise ingress has been taken from Approved Document E.

3.9 The development will require pre-completion sound insulation testing under Approved Document E 2015 of The Building Regulations 2010. The performance requirements of Approved Document E are detailed below:

Table 0.1a Dwelling-houses and flats – performance standards for separating walls, separating floors, and stairs that have a separating function

Purpose built dwelling-houses and flats	Airborne sound insulation sound insulation $D_{nT,w} + C_{tr}$ dB (Minimum values)	Impact sound insulation $L_{nT,w}$ dB (Maximum values)
Walls	45	-
Floors and stairs	45	62
Dwelling-houses and flats formed by material change of use		
Walls	43	-
Floors and stairs	43	64

3.10 The site can be categorised as new build “*purpose built dwelling - houses and flats*” under Approved Document E 2015 of the Building Regulations 2010. Purpose built dwelling-houses and flats, the minimum airborne performance is  $D_{nT,w} + C_{tr}$  45dB.

3.11 Given the nature of the possible ground floor commercial use and the potential for higher than normal domestic noise levels to be generated, it is recommended that an enhanced performance is targeted.

3.12 In this instance it would be reasonable to target +10dB better than the minimum performance requirements of Approved Document E, so the enhanced minimum airborne performance targeted would be  $D_{nT,w} + C_{tr}$  55dB ( $D_{nT,w} + C_{tr}$  45dB+10dB).

## 4. NOISE OUTLINE

4.1 In order to determine the environmental noise level, consideration has been given to the noise levels on the site from the presence of commercial/transportation noise impacting the site.

4.2 Unmanned measurements were obtained over a 24 hour period at first floor level at the front and rear of the site, these locations were chosen to represent worst case noise levels that would be experienced at the façades of the proposed new residential accommodation from noise sources impacting the development.

4.3 The particulars of the measurement exercise are recorded below:

Date: 2<sup>nd</sup> – 3<sup>rd</sup> June 2025  
Start Time: 11:30 hrs  
Location: First floor level at front and rear of site.

4.4 The measurements carried out during the exercise are recorded below.

$L_{Aeq, 2mins}$  (dB re 20 $\mu$ Pa) - average equivalent sound pressure level  
 $L_{Max, 2mins}$  (dB re 20 $\mu$ Pa) – maximum sound pressure level.

4.5 A level vs time summary of the noise data obtained at the site is presented in Diagrams 2 and 3.

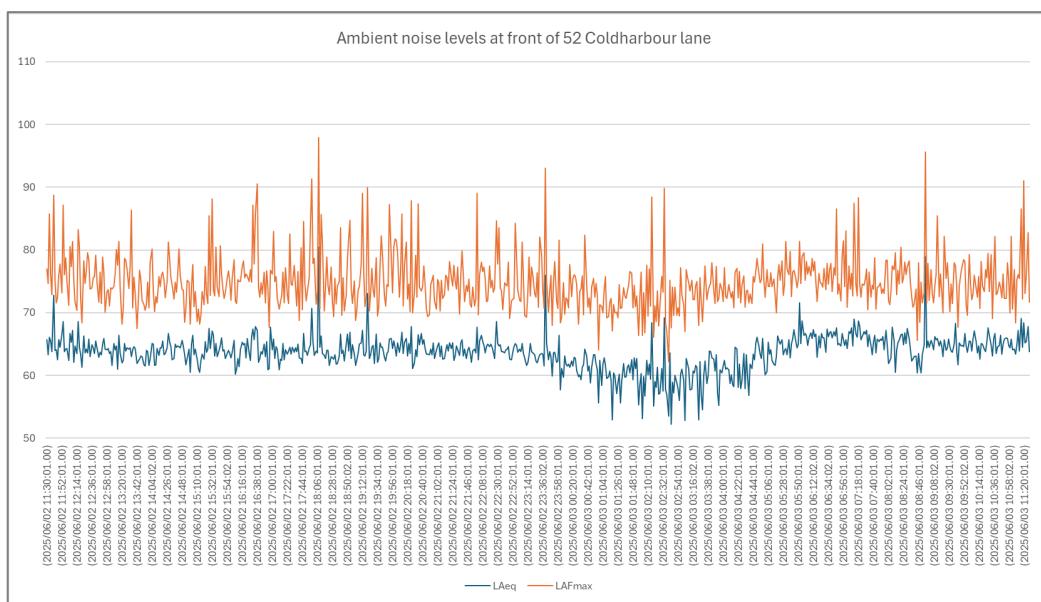


Diagram 2 – level vs time history at front of the site

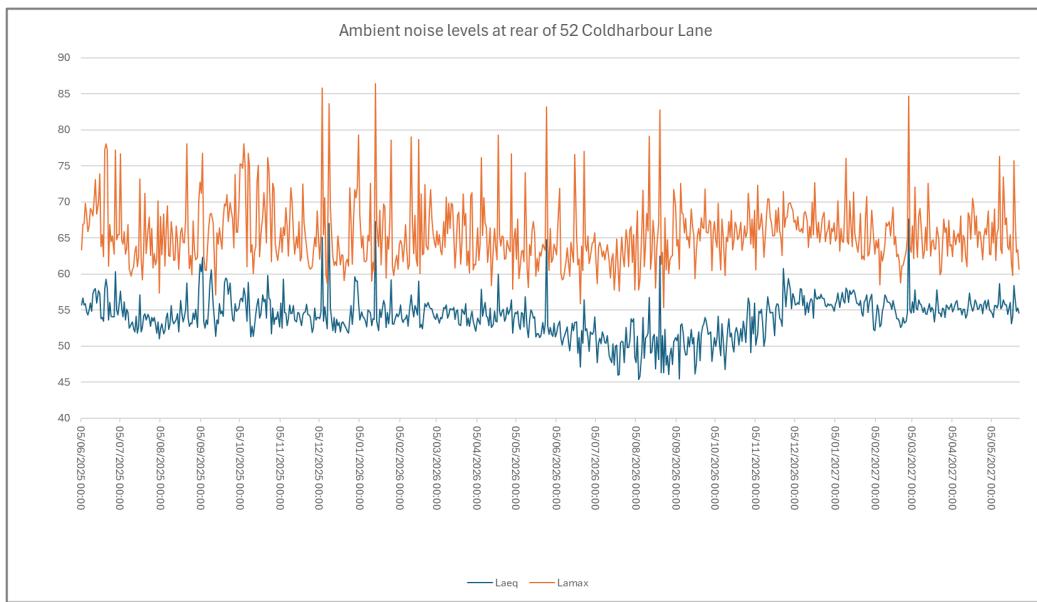


Diagram 3 – level vs time history at rear of the site

## 5. EQUIPMENT

5.1 All measurements were obtained using the following equipment. The relevant equipment carries full and current traceable calibration. The equipment, where necessary, was calibrated prior to and after the measurements were carried out.

- *Norsonic NOR-140 Serial No. 1403466*
- *Rion NA28 Serial No. 00370311*
- *Rion Calibrator Type NC-74 Class 1 Serial No. 00410215*

## 6. BUILDING ENVELOPE ASSESSMENT

- 6.1 Given the monitoring position and the measurements obtained, it is possible to calculate the  $L_{Aeq,T}$  values experienced during the experienced during the day and night-time periods.
- 6.2 For the purposes of this report and in line with the recommendation of BS8233, the following time periods have been calculated.
  - (a) 07:00 hrs to 23:00 hrs for living rooms/dining rooms.
  - (b) 23:00 hrs to 07:00 hrs for bedrooms.
- 6.3 The measurements are based on the day and night time period  $L_{Aeq,2min}$  and  $L_{Amax,2mins}$  measurements obtained during the measurement exercise at the site. The results obtained are detailed below.

Location	Daytime 07:00 to 23:00hrs	Night time 23:00 to 07:00hrs	15 <sup>th</sup> highest <sup>1</sup> $L_{Amax}$ dB
Front	65dB	63dB	79dB
Rear	56dB	54dB	71dB

Table 2

## 7. BUILDING ENVELOPE RECOMMENDATIONS

- 7.1 It is recommended that in order to address the internal noise requirements of BS8233:2014, acoustic fenestration measures will be considered in order to protect the daytime and night-time amenity of future occupiers.
- 7.2 This should minimise future residents complaining about noise from urban traffic movements and commercial activity noise in the neighbourhood.
- 7.3 It has been determined that passive background ventilation is to be provided to the new residential dwellings. The internal noise requirements of BS8233 can only be met with windows closed.

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<sup>1</sup> From the data, the 15<sup>th</sup> highest  $L_{Amax,F}$  measurement during the night time period at the façade has been considered, this is taken from WHO Guidelines for Community Noise – which states “For a good sleep, it is believed that indoor sound pressure levels should not exceed approximately 45dB  $L_{Amax}$  more than 10-15 times per night” (Vallet and Vernet 1991).

7.4 To reduce daytime and night-time noise exposure in the proposed dwellings, attention should be given to the sound insulation of the façade of the building. The windows will normally be the weakest part of any façade.

7.5 Based on the outline information supplied, it is anticipated the external wall, mansard and roof constructions on site will have insulation values as detailed in Table 3 below. These performance values were obtained from proprietary prediction software 'Insul' written by Marshall Day. The values predicted have been corrected to account for workmanship, onsite installation and the differences between lightweight and heavyweight construction systems.

Construction	Insulation value	Prediction correction
External wall (cavity masonry)	R <sub>w</sub> 52dB	-4dB
Mansard wall (steel frame)	R <sub>w</sub> 66dB	-7dB
Roof (warm type roof)	R <sub>w</sub> 64dB	-7dB

Table 3

7.6 A copy of the prediction outputs for the noted constructions are contained within Appendix A of this report. Given the external noise levels, it is essential that the glazing performances as calculated are met. This will provide the necessary sound insulation values to reduce the internal noise levels to an acceptable level.

7.7 If the constructions were to be revised, the performance values should be checked prior to the change of use, to ensure the internal noise level requirements of BS8233:2014 are still met.

7.8 From the calculated levels it is possible to predict the internal noise levels within habitable rooms. In order to undertake this, consideration has been given to the following formula:

$$SPL_{in} = SPL_{out} + 10\log_{10} \left( \frac{A_0}{S} 10^{\frac{-D_{n,e}}{10}} + \frac{S_{wi}}{S} 10^{\frac{-R_{wi}}{10}} + \frac{S_{ew}}{S} 10^{\frac{-R_{ew}}{10}} + \frac{S}{A} \right) + 3$$

where:

SPL <sub>in</sub> =	sound pressure level inside the room
SPL <sub>out</sub> =	highest sound pressure level outside the room
A <sub>0</sub> =	reference absorption area of 10m <sup>2</sup>
S <sub>wi</sub> =	area in m <sup>2</sup> of the windows of the room
S <sub>ew</sub> =	area in m <sup>2</sup> of the external wall of the room
R <sub>wi</sub> =	weighted sound reduction index of window (R <sub>w</sub> +C <sub>ir</sub> )
R <sub>ew</sub> =	weighted sound reduction index of external wall
S =	area through which sound is transmitted (m <sup>2</sup> )
A =	amount of acoustic absorption in room (m <sup>2</sup> )
K =	a numerical factor associated with sound incidence

Equation 1

7.9 Room dimensions and the size of windows have been extracted from scaled drawings. For the purposes of the calculation exercises, the accommodation types proposed at each level has been assessed.

7.10 Due to the varying methods of quantifying the sound insulation performance of building elements, the following parameters are described:

- $R_w$  Weighted Sound Reduction Index: Single figure sound insulation value derived from the measured sound reduction index  $R$ .

7.11 To meet the criteria, Equation 1 was rearranged in terms of  $R_w$  (the sound reduction index of the window). The window specification required in order to achieve the internal noise levels as set out in BS8233 is shown in Table 4. Details of the elements assessed within the calculation exercises are contained within Appendix B of this report.

Location	Sound Reduction Index ( $R_w$ )	$D_{n,e,w}$
Levels 01 & 02 habitable rooms (front)	35dB	55dB
Level 03 habitable rooms (front)	35dB	39dB
Levels 01, 02 & 03 all habitable rooms (rear)	34dB	33dB

Table 4

7.12 To achieve the values of  $R_w$  as specified in Table 4, a number of glazing systems were reviewed. The required window performance can be achieved using the following glazing configuration (taken from Guardian Glass):

Required window performance	Glazing configuration (example)
34dB $R_w$	6mm float glass 10mm cavity 4mm Float glass
35dB $R_w$	8mm float glass 10mm cavity 6mm Float glass

Table 5

7.13 The suggested window specification is detailed in Appendix C. This glass has published performance data. The published performance figures for the 'glass only' were obtained from laboratory measurements. The best workmanship practices and installation guidelines should be followed to ensure that the stated performances can be obtained once installed within a frame.

7.14 To achieve the  $D_{n,e,w}$ , as specified in Table 4, a Simon Acoustics frame ventilator ( $D_{n,e,w}$  33dB), Greenwood AWV39 wall ventilator ( $D_{n,e,w}$  39dB) or Greenwood MA3051 wall vent ( $D_{n,e,w}$  55dB) was used. Other frame or wall vents with equal or better performance are available. For the benefit of the calculation exercise, 2no. vents were assumed for the living room and 1no. vent for the bedroom spaces.

7.15 Alternatively, a window system (glass and frame) matching or exceeding the octave band performances detailed within the calculation exercises (Appendix B) would be acceptable, the minimum octave band performance levels required for any window system (glass and frame) are confirmed below in Table 6.

Minimum performance requirements	SRI Octave Band Centre Frequency (Hz) dB								R <sub>w</sub>
	63	125	250	500	1k	2k	4k	8k	
34dB R <sub>w</sub>	-	27	26	28	37	36	29	-	34dB
35dB R <sub>w</sub>	-	30	27	29	38	35	35	-	35dB

Table 6

## VENTILATION

7.16 Ventilation requirements for dwellings (and other buildings) are covered under the Building Regulations 'Approved Document F – Means of Ventilation, 2010 Volume 1:Dwellings (ADF).

7.17 ADF requires that: "There shall be adequate means of ventilation provided for people in the building".

7.18 Ventilation is required for the following purposes:

- Extracts water vapour and indoor pollutants from areas where they are produced in significant quantities.*
- Supplies a minimum level of outdoor air for occupants' health.*
- Rapidly dilutes indoor air pollutants and disperses water vapour when necessary.*

7.19 ADF describes three types of ventilation provision and associated use. The types of ventilation are summarised below:

Type of ventilation	Location	When is this required
Extract Ventilation	Kitchens Utility rooms Bathrooms Sanitary accommodation	Continuous or Intermittent
Whole Dwelling Ventilation	All habitable rooms	Continuously
Purge Ventilation	All habitable rooms	Occasionally

Table 7

7.20 It is currently proposed to install 'extract ventilation' to the residential units. In addition to the above ADF also states:

*"Purge ventilation should be capable of extracting at least four air changes per hour per room directly to the outside."*

7.21 If required to demonstrate compliance with Part O of the Building Regulations, it is likely that higher purge ventilation rates than those given above will be required.

## 8. GROUND FLOOR COMMERCIAL NOISE INGRESS

- 8.1 In order to produce a noise assessment to demonstrate that noise when considering the proposed 'ground floor commercial use and to mitigate and minimise any potential adverse impact of noise, as a result of the new development. Consideration must be given to the typical noise levels likely to be generated within the commercial use at ground floor level.
- 8.2 It has been assumed that the ground floor commercial unit could generate higher than normal domestic noise levels given the large open plan workplace. The recommended enhanced performance for the floor construction separating the commercial and residential elements has been targeted to achieve an airborne performance of  $D_{nT,w} + C_{tr}$  55dB.
- 8.3 The materials and construction methods are yet to be finalised but when the scheme details are confirmed during the detailed design stage, a suggested enhanced airborne performance of  $D_{nT,w} + C_{tr}$  55dB can be achieved.

## 9. CONCLUSION

- 9.1 With regard to the permitted development, it can be concluded that:
  - (a) *The general noise climate was impacted by commercial activity and urban traffic movements at the front and rear of the site.*
- 9.2 Based on the foregoing building envelope assessment, it can be concluded that:
  - (a) *Glazing systems with the appropriate acoustic performance (Table 4) would provide sufficient attenuation from noise levels impacting the site and reduce internal noise levels to not exceed the upper limit levels stated within ProPG, BS 8233:2014 and WHO guidelines for Community Noise.*
  - (b) *The required level of sound insulation needed to achieve this internal level is based on the building envelope make up considered.*
  - (c) *Passive ventilation is proposed for the residential units to provide adequate background ventilation and to avoid having to open windows. Ventilators with the relevant acoustic performance (Table 4) would provide sufficient attenuation to reduce internal noise levels to meet the minimum requirements recommended within ProPG, BS8233:2014 and World Health Organisation (WHO) guidelines.*
- 9.3 Ground floor commercial noise ingress will target an airborne performance target of  $D_{nT,w} + C_{tr}$  55dB to separate the different uses at ground and first floor level, evidence of the construction method will be provided during the detailed design stage.

## **Figures**

**52 Coldharbour Lane, Hayes, UB3 3EP.**



Figure 1



Figure 2



Figure 3



Figure 4



Figure 5



Figure 6

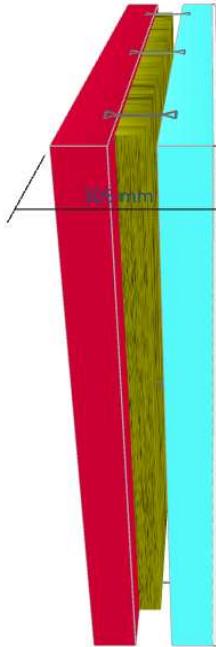


Figure 7



Figure 8

## **Appendix A**



**$R_w$  52 dB**  
 C -1 dB  
 Ctr -4 dB

Mass-air-mass resonant frequency = =23 Hz

Panel Size = 2.7 m x 4.0 m

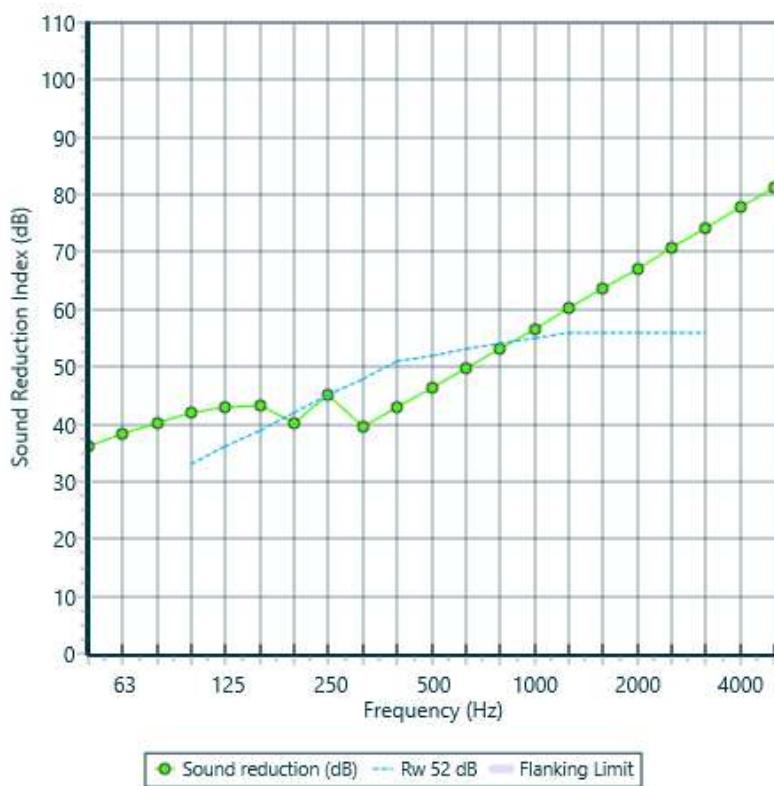
Partition surface mass = 253 kg/m<sup>2</sup>

## System description

Panel 1 : 1 x 102.5 mm Brick

Frame: Butterfly Tie (90 mm x 45 mm), Stud spacing 600 mm ; Cavity Width 90 mm , 1 x Fibreglass (10kg/m3) 60mm Thickness 60 mm  
 Panel 2 : 1 x 100 mm blockwork 800kg density + 1 x 12.5 mm Gyproc Wallboard 12.5mm

freq.(Hz)	R(dB)	R(dB)
50	36	
63	38	38
80	40	
100	42	
125	43	43
160	43	
200	40	
250	45	41
315	40	
400	43	
500	46	46
630	50	
800	53	
1000	57	56
1250	60	
1600	64	
2000	67	66
2500	71	
3150	74	
4000	78	77
5000	81	





**$R_w$  66 dB**  
 C -3 dB  
 Ctr -7 dB

Mass-air-mass resonant frequency = =36 Hz

Panel Size = 2.7 m x 4.0 m

Partition surface mass = 58.1 kg/m<sup>2</sup>

## System description

Panel 1 : 1 x 1 mm Copper

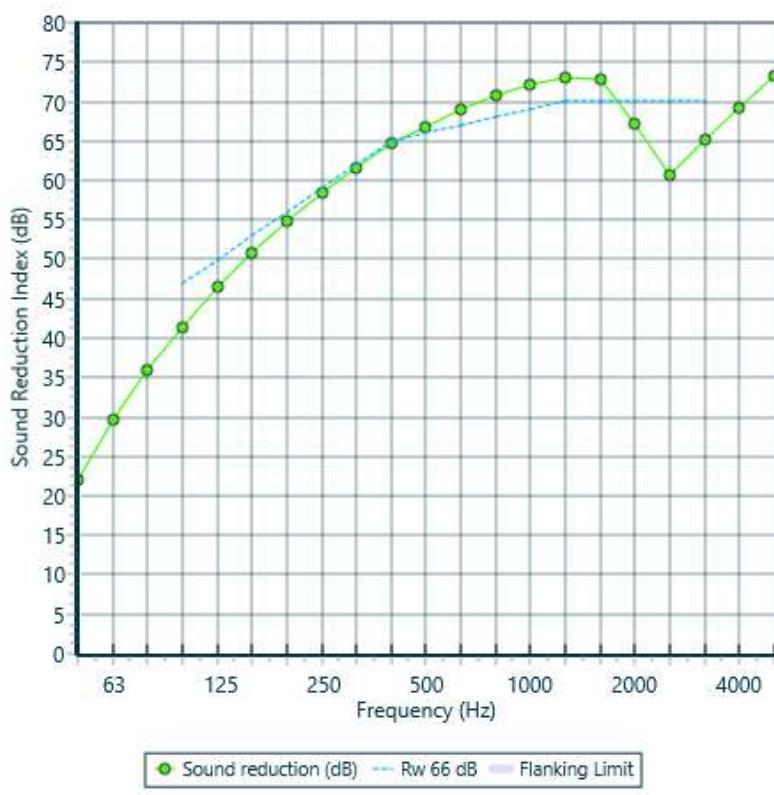
+ 1 x 18 mm RCM CemBoard (cement particle board)

Frame: Steel Stud + resil. rail (1.4E2 mm x 38 mm), Stud spacing 600 mm ; Cavity Width 150 mm , 1 x Fibreglass (10kg/m3) 60mm Thickness 100 mm

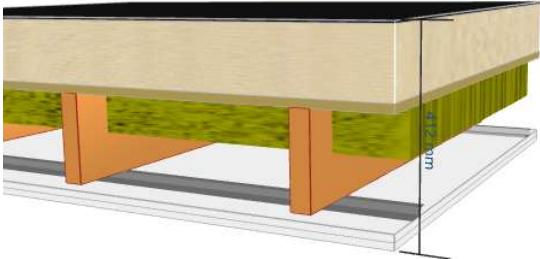
Panel 2 : 2 x 15 mm Gyproc SoundBloc 15mm

...

freq.(Hz)	$R$ (dB)	$R$ (dB)
50	22	
63	30	26
80	36	
100	41	
125	46	45
160	51	
200	55	
250	58	57
315	62	
400	65	
500	67	66
630	69	
800	71	
1000	72	72
1250	73	
1600	73	
2000	67	64
2500	61	
3150	65	
4000	69	68
5000	73	



Notes:Third floor roof



**R<sub>w</sub> 64 dB**  
 C -1 dB  
 Ctr -5 dB

Mass-air-mass resonant frequency = =28 Hz

Panel Size = 2.7 m x 4.0 m

Partition surface mass = 67.8 kg/m<sup>2</sup>

## System description

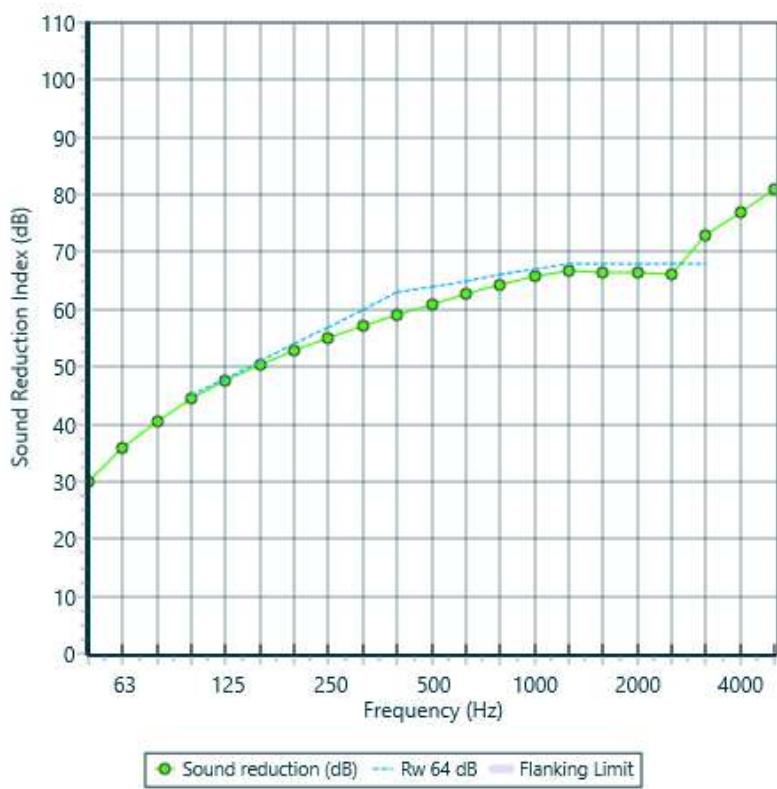
Panel 1 : 1 x 4 mm Nuraply waterproof membrane  
 + 1 x 18 mm RCM CemBoard (cement particle board)

+ 1 x 139.9 mm Kingspan KS 1000AWP 120/140mm

Frame: Solid Joist with resilient rail (2E2 mm x 45 mm), Stud spacing 600 mm ; Cavity Width 220 mm , 1 x Fibreglass (10kg/m<sup>3</sup>) 60mm Thickness 100 mm  
 Panel 2 : 2 x 15 mm Gyproc SoundBloc 15mm

...

freq.(Hz)	R(dB)	R(dB)
50	30	
63	36	34
80	41	
100	44	
125	48	47
160	50	
200	53	
250	55	55
315	57	
400	59	
500	61	61
630	63	
800	64	
1000	66	66
1250	67	
1600	66	
2000	67	66
2500	66	
3150	73	
4000	77	76
5000	81	



## **Appendix B**

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{eq,ff}$	65dB(A)	67	64	61	58	52
2no. Passive ventilators MA3051	$D_{ne,w}$	Dne,w 55dB	50	48	51	56	67
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	38	35
External wall	$R_{ew}$	Rw 52 dB	39	37	42	52	73
Roof	$R_{rr}$	Rw n/a dB	100	100	100	100	100
Total room absorption (based on RT)	$RT_{60}$	0.8	13	15	17	17	16

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	33					
Window area	$S_{wi}$	10					
$S_f - S_{wi}$	$S_{ew}$	23					
Area of ceiling	$S_{tr}$	33					
$S_f + S_{tr}$	$S$	66					
Reference absorption area	$A_0$	10					
Room volume	$V$	82					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	67	64	61	61	58
2no. Passive ventilators MA3051	$D_{ne,e}$		49.76091259	47.76091259	50.76091259	55.76091259	66.76091259
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00000	0.00000	0.00000	0.00000	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00031	0.00020	0.00002	0.00005
External Wall Construction	$R_{ew}$		39	37	42	52	62
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00004	0.00007	0.00002	0.00000	0.00000
Roof Construction	$R_{rr}$		100	100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-34	-37	-46	-43
Total Absorption Area of Receiver Room	A (furnished)		13	15	17	17	16
	$10\log(S/A)$	G	7.2	6.5	6.0	6.2	6.2
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	40.5	39.9	33.6	24.4	23.8

**RESULTANT INTERNAL NOISE LEVEL** 35

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{eq,ff}$	65dB(A)	67	64	61	58	52
Passive Ventilation MA3051	$D_{ne,w}$	Dne,w 55dB	53	51	54	59	71
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	38	35
External wall	$R_{ew}$	Rw 52 dB	39	37	42	52	73
Roof	$R_{rr}$	Rw n/a dB	100	100	100	100	100
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	7	9	11	11	10

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	11					
Window area	$S_{wi}$	4					
$S_f - S_{wi}$	$S_{ew}$	7					
Area of ceiling	$S_{tr}$	13					
$S_f + S_{tr}$	$S$	24					
Reference absorption area	$A_0$	10					
Room volume	$V$	33					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	67	64	61	61	58
Passive Ventilation MA3051	$D_{ne,e}$		52.77121255	50.77121255	53.77121255	58.77121255	69.77121255
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00000	0.00000	0.00000	0.00000	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00015	0.00030	0.00019	0.00002	0.00005
External Wall Construction	$R_{ew}$		39	37	42	52	62
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00004	0.00006	0.00002	0.00000	0.00000
Roof Construction	$R_{rr}$		100	100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-34	-37	-46	-43
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10
	$10\log(S/A)$	G	5.5	4.4	3.5	3.5	3.9
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	38.6	37.5	30.9	21.7	15.2

**RESULTANT INTERNAL NOISE LEVEL** 33

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{eq,ff}$	63dB(A)	65	62	58	60	56
Passive Ventilation MA3051	$D_{ne,w}$	Dne,w 55dB	53	51	54	59	70
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	38	35
External wall	$R_{ew}$	Rw 52 dB	39	37	42	52	62
Roof	$R_{rr}$	Rw n/a dB	100	100	100	100	100
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	7	9	11	11	10

Derivation	Term	Value
Facade area (including window)	$S_f$	11
Window area	$S_{wi}$	4
$S_f - S_{wi}$	$S_{ew}$	7
Area of ceiling	$S_{tr}$	13
$S_f + S_{tr}$	$S$	24
Reference absorption area	$A_0$	10
Room volume	$V$	33

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	65	62	58	60	56
Passive Ventilation MA3051	$D_{ne,e}$		52.77121255	50.77121255	53.77121255	58.77121255	69.77121255
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00000	0.00000	0.00000	0.00000	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00015	0.00030	0.00019	0.00002	0.00005
External Wall Construction	$R_{ew}$		39	37	42	52	62
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00004	0.00006	0.00002	0.00000	0.00000
Roof Construction	$R_{rr}$		100	100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-34	-37	-46	-43
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10
	$10\log(S/A)$	G	5.5	4.4	3.5	3.5	3.9
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	36.0	35.0	27.7	20.6	19.7

RESULTANT INTERNAL NOISE LEVEL

30

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{max,ff}$	80dB(A)	72	69	76	79	67
Passive Ventilation MA3051	$D_{ne,w}$	$D_{ne,w} 55dB$	53	51	54	59	70
Glazing 8mm float / 10mm / 6mm float	$R_w$	$R_w 35dB$	30	27	29	38	35
External wall	$R_{ew}$	$R_w 52dB$	39	37	42	52	62
Roof	$R_{rr}$	$R_w n/a dB$	100	100	100	100	100
Total room absorption (based on RT)	$RT_{60}$	0.5	7	9	11	11	10

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	11					
Window area	$S_{wi}$	4					
$S_f - S_{wi}$	$S_{ew}$	7					
Area of ceiling	$S_{tr}$	13					
$S_f + S_{tr}$	$S$	24					
Reference absorption area	$A_0$	10					
Room volume	$V$	33					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	72	69	76	79	67
Passive Ventilation MA3051	$D_{ne,e}$		52.77121255	50.77121255	53.77121255	58.77121255	69.77121255
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00000	0.00000	0.00000	0.00000	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00015	0.00030	0.00019	0.00002	0.00005
External Wall Construction	$R_{ew}$		39	37	42	52	62
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00004	0.00006	0.00002	0.00000	0.00000
Roof Construction	$R_{rr}$		100	100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-34	-37	-46	-43
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10
	$10\log(S/A)$	G	5.5	4.4	3.5	3.5	3.9
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	43.7	42.2	46.0	39.4	30.8

RESULTANT INTERNAL NOISE LEVEL

45

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Rear	$L_{eq,ff}$	56dB(A)	59	56	51	52	47
2no. Simon Acoustic frame ventilators	$D_{ne,w}$	Dne,w 33dB	36	33	32	28	29
Glazing 6mm float / 10mm / 4mm float	$R_w$	Rw 34dB	27	26	28	37	36
External wall	$R_{ew}$	Rw 52 dB	39	37	42	52	62
Roof	$R_{rr}$	Rw n/a dB	100	100	100	100	100
Total room absorption (based on RT)	RT <sub>60</sub>	0.8	9	11	13	13	12

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	27					
Window area	$S_{wi}$	4					
$S_f - S_{wi}$	$S_{ew}$	23					
Area of ceiling	$S_{tr}$	25					
$S_f + S_{tr}$	$S$	52					
Reference absorption area	$A_0$	10					
Room volume	$V$	63					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	59	56	51	52	47
2no. Simon Acoustic frame ventilators	$D_{ne,e}$	$D_{ne,w}$	36.48970004	32.88970004	32.08970004	27.68970004	29.08970004
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00004	0.00010	0.00012	0.00033	0.00024
Double Glazed Windows	$R_{wi}$	$R_{ew}$	27	26	28	37	36
External Wall Construction	$R_{ew}$	$R_{tr}$	0.00016	0.00020	0.00013	0.00002	0.00002
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	C	39	37	42	52	62
Roof Construction	$R_{tr}$	$R_{rr}$	0.00006	0.00009	0.00003	0.00000	0.00000
	$(S_{tr}/S)*10^{A(-R_{tr}/10)}$	D	100	100	100	100	100
Total Sound Insulation Performance	$10\log(B+C+D+E)$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Absorption Area of Receiver Room	A (furnished)	F	-36	-34	-36	-35	-36
	$10\log(S/A)$	G	9	11	13	13	12
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	34.1	31.5	24.9	26.5	20.4

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)			
			125	250	500	1000
Freefield External Noise Level - Rear	$L_{eq,ff}$	56dB(A)	59	56	51	52
Simon Acoustic frame ventilator	$D_{ne,w}$	Dne,w 33dB	40	36	35	31
Glazing 6mm float / 10mm / 4mm float	$R_w$	Rw 34dB	27	26	28	37
External wall	$R_{ew}$	Rw 52 dB	39	37	42	52
Roof	$R_{rr}$	Rw n/a dB	100	100	100	100
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	7	9	11	11

Derivation	Term	Value
Facade area (including window)	$S_f$	12
Window area	$S_{wi}$	2
$S_f - S_{wi}$	$S_{ew}$	10
Area of ceiling	$S_{tr}$	13
$S_f + S_{tr}$	$S$	26
Reference absorption area	$A_0$	10
Room volume	$V$	33

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)			
			125	250	500	1000
Freefield External Noise Level	$L_{eq,ff}$	A	59	56	51	52
Simon Acoustic frame ventilator	$D_{ne,e}$		39.5	35.9	35.1	30.7
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00004	0.00010	0.00012	0.00033
Double Glazed Windows	$R_{wi}$		27	26	28	37
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00021	0.00013	0.00002
External Wall Construction	$R_{ew}$		39	37	42	52
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00005	0.00008	0.00003	0.00000
Roof Construction	$R_{rr}$		100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-36	-34	-36	-35
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11
	$10\log(S/A)$	G	5.7	4.6	3.7	4.1
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	32.0	29.3	22.5	18.2

**RESULTANT INTERNAL NOISE LEVEL** 28

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Rear	$L_{eq,ff}$	54dB(A)	57	53	48	51	44
Simon Acoustic frame ventilator	$D_{ne,w}$	Dne,w 33dB	40	36	35	31	32
Glazing 6mm float / 10mm / 4mm float	$R_w$	Rw 34dB	27	26	28	37	36
External wall	$R_{ew}$	Rw 52 dB	39	37	42	52	62
Roof	$R_{rr}$	Rw n/a dB	100	100	100	100	100
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	7	9	11	11	10

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	12					
Window area	$S_{wi}$	2					
$S_f - S_{wi}$	$S_{ew}$	10					
Area of ceiling	$S_{tr}$	13					
$S_f + S_{tr}$	$S$	26					
Reference absorption area	$A_0$	10					
Room volume	$V$	33					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	57	53	48	51	44
Simon Acoustic frame ventilator	$D_{ne,e}$		39.5	35.9	35.1	30.7	32.1
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00004	0.00010	0.00012	0.00033	0.00024
Double Glazed Windows	$R_{wi}$		27	26	28	37	36
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00021	0.00013	0.00002	0.00002
External Wall Construction	$R_{ew}$		39	37	42	52	62
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00005	0.00008	0.00003	0.00000	0.00000
Roof Construction	$R_{rr}$		100	100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-36	-34	-36	-35	-36
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10
	$10\log(S/A)$	G	5.7	4.6	3.7	4.1	4.1
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	29.5	26.8	19.6	22.9	15.7

RESULTANT INTERNAL NOISE LEVEL

26

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Rear	$L_{max,ff}$	72dB(A)	70	68	63	70	63
Simon Acoustic frame ventilator	$D_{ne,w}$	$D_{ne,w} 33dB$	40	36	35	31	32
Glazing 6mm float / 10mm / 4mm float	$R_w$	$R_w 34dB$	27	26	28	37	36
External wall	$R_{ew}$	$R_w 52dB$	39	37	42	52	62
Roof	$R_{rr}$	$R_w n/a dB$	100	100	100	100	100
Total room absorption (based on RT)	$RT_{60}$	0.5	7	9	11	11	10

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	12					
Window area	$S_{wi}$	2					
$S_f - S_{wi}$	$S_{ew}$	10					
Area of ceiling	$S_{tr}$	13					
$S_f + S_{tr}$	$S$	26					
Reference absorption area	$A_0$	10					
Room volume	$V$	33					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	70	68	63	70	63
Simon Acoustic frame ventilator	$D_{ne,e}$		39.5	35.9	35.1	30.7	32.1
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00004	0.00010	0.00012	0.00033	0.00024
Double Glazed Windows	$R_{wi}$		27	26	28	37	36
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00021	0.00013	0.00002	0.00002
External Wall Construction	$R_{ew}$		39	37	42	52	62
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00005	0.00008	0.00003	0.00000	0.00000
Roof Construction	$R_{rr}$		100	100	100	100	100
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00000	0.00000	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-36	-34	-36	-35	-36
Total Absorption Area of Receiver Room	A (furnished)		7	9	11	11	10
	$10\log(S/A)$	G	5.7	4.6	3.7	4.1	4.1
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	42.5	41.1	42.2	34.0	21.3

**RESULTANT INTERNAL NOISE LEVEL** 44

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{eq,ff}$	65dB(A)	67	64	61	58	52
Greenwoods AWV 39 ventilator x2	$D_{ne,w}$	Dne,w 39dB	41	38	38	49	61
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	38	35
External wall - Mansard	$R_{ew}$	Rw 66 dB	38	50	59	65	61
Roof	$R_{rr}$	Rw 64 dB	40	48	54	59	69
Total room absorption (based on RT)	RT <sub>60</sub>	0.8	10	12	14	14	13

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	29					
Window area	$S_{wi}$	4					
$S_f - S_{wi}$	$S_{ew}$	25					
Area of ceiling	$S_{tr}$	27					
$S_f + S_{tr}$	$S$	56					
Reference absorption area	$A_0$	10					
Room volume	$V$	68					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	67	64	61	61	58
Greenwoods AWV 39 ventilator x2	$D_{ne,e}$		40.76091259	37.76091259	39.76091259	48.76091259	60.76091259
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00002	0.00003	0.00003	0.00002	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00008	0.00015	0.00009	0.00001	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65	57
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-37	-39	-45	-46
Total Absorption Area of Receiver Room	A (furnished)		10	12	14	14	13
	$10\log(S/A)$	G	7.6	6.8	6.1	6.4	6.4
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	41.1	37.1	31..3	25.1	14.8

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{eq,ff}$	65dBA	67	64	61	58	52
Greenwoods AWV 39 ventilator	$D_{ne,w}$	Dne,w 39dB	44	41	43	52	64
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	35	35
External wall - Mansard	$R_{ew}$	Rw 66 dB	38	50	59	65	61
Roof	$R_{rr}$	Rw 64 dB	40	48	54	59	69
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	16	18	20	20	19

Derivation	Term	Value
Facade area (including window)	$S_f$	26
Window area	$S_{wi}$	3
$S_f - S_{wi}$	$S_{ew}$	23
Area of ceiling	$S_{tr}$	24
$S_f + S_{tr}$	$S$	50
Reference absorption area	$A_0$	10
Room volume	$V$	61

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	67	64	61	61	58
Greenwoods AWV 39 ventilator	$D_{ne,e}$		43.77121255	40.77121255	42.77121255	51.77121255	63.77121255
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00001	0.00002	0.00002	0.00001	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00006	0.00013	0.00008	0.00001	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65	57
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-38	-40	-47	-46
Total Absorption Area of Receiver Room	A (furnished)		16	18	20	20	19
	$10\log(S/A)$	G	5.0	4.5	4.0	4.3	4.3
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	38.2	33.9	28.2	21.4	18.5

RESULTANT INTERNAL NOISE LEVEL

30

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{eq,ff}$	63dB(A)	65	62	58	60	56
Greenwoods AWV 39 ventilator	$D_{ne,w}$	Dne,w 39dB	44	41	41	43	52
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	38	35
External wall - Mansard	$R_{ew}$	Rw 66 dB	38	50	59	65	57
Roof	$R_{rr}$	Rw 64 dB	40	48	54	59	59
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	16	18	20	20	19

Derivation	Term	Value
Facade area (including window)	$S_f$	26
Window area	$S_{wi}$	3
$S_f - S_{wi}$	$S_{ew}$	23
Area of ceiling	$S_{tr}$	24
$S_f + S_{tr}$	$S$	50
Reference absorption area	$A_0$	10
Room volume	$V$	61

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	65	62	58	60	56
Greenwoods AWV 39 ventilator	$D_{ne,e}$		43.77121255	40.77121255	42.77121255	51.77121255	63.77121255
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00001	0.00002	0.00002	0.00001	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00006	0.00013	0.00008	0.00001	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65	57
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-38	-40	-47	-46
Total Absorption Area of Receiver Room	A (furnished)		16	18	20	20	19
	$10\log(S/A)$	G	5.0	4.5	4.0	4.3	4.3
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	35.6	31.4	25.0	20.2	16.9

RESULTANT INTERNAL NOISE LEVEL

28

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Front	$L_{max,ff}$	80dBA	72	69	76	79	67
Greenwoods AWV 39 ventilator	$D_{ne,w}$	Dne,w 39dB	44	41	41	43	52
Glazing 8mm float / 10mm / 6mm float	$R_w$	Rw 35dB	30	27	29	38	35
External wall - Mansard	$R_{ew}$	Rw 66 dB	38	50	59	65	57
Roof	$R_{rr}$	Rw 64 dB	40	48	54	59	59
Total room absorption (based on RT)	$RT_{60}$	0.5	16	18	20	20	19

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	26					
Window area	$S_{wi}$	3					
$S_f - S_{wi}$	$S_{ew}$	23					
Area of ceiling	$S_{tr}$	24					
$S_f + S_{tr}$	$S$	50					
Reference absorption area	$A_0$	10					
Room volume	$V$	61					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	72	69	76	79	67
Greenwoods AWV 39 ventilator	$D_{ne,e}$		43.77121255	40.77121255	42.77121255	51.77121255	63.77121255
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00001	0.00002	0.00002	0.00001	0.00000
Double Glazed Windows	$R_{wi}$		30	27	29	38	35
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00006	0.00013	0.00008	0.00001	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65	57
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-37	-38	-40	-47	-46
Total Absorption Area of Receiver Room	A (furnished)		16	18	20	20	19
	$10\log(S/A)$	G	5.0	4.5	4.0	4.3	4.3
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	43.2	38.6	43.3	39.0	27.9

RESULTANT INTERNAL NOISE LEVEL

43

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Rear	$L_{eq,ff}$	56dB(A)	59	56	51	52	47
Simon Acoustic frame ventilator	$D_{ne,w}$	Dne,w 33dB	40	36	35	31	32
Glazing 6mm float / 10mm / 4mm float	$R_w$	Rw 34dB	27	26	28	37	36
External wall - Mansard	$R_{ew}$	Rw 66 dB	38	50	59	65	57
Roof	$R_{rr}$	Rw 64 dB	40	48	54	59	59
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	13	15	17	17	16

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	23					
Window area	$S_{wi}$	4					
$S_f - S_{wi}$	$S_{ew}$	20					
Area of ceiling	$S_{tr}$	21					
$S_f + S_{tr}$	$S$	44					
Reference absorption area	$A_0$	10					
Room volume	$V$	52					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	59	56	51	52	47
Simon Acoustic frame ventilator	$D_{ne,e}$		39.5	35.9	35.1	30.7	32.1
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00003	0.00006	0.00007	0.00019	0.00014
Double Glazed Windows	$R_{wi}$		27	26	28	37	36
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00020	0.00013	0.00002	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65	57
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-35	-36	-37	-37	-38
Total Absorption Area of Receiver Room	A (furnished)		13	15	17	17	16
	$10\log(S/A)$	G	5.3	4.7	4.1	4.1	4.4
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	32.3	27.9	21.6	22.4	16.3

RESULTANT INTERNAL NOISE LEVEL

26

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)			
			125	250	500	1000
Freefield External Noise Level - Rear	$L_{eq,ff}$	54dB(A)	57	53	48	51
Simon Acoustic frame ventilator	$D_{ne,w}$	Dne,w 33dB	40	36	35	31
Glazing 6mm float / 10mm / 4mm float	$R_w$	Rw 34dB	27	26	28	37
External wall - Mansard	$R_{ew}$	Rw 66 dB	38	50	59	65
Roof	$R_{rr}$	Rw 64 dB	40	48	54	59
Total room absorption (based on RT)	RT <sub>60</sub>	0.5	13	15	17	17
						16
						16

Derivation	Term	Value	Octave Band Centre Frequency (Hz)			
			125	250	500	1000
Facade area (including window)	$S_f$	23				
Window area	$S_{wi}$	4				
$S_f - S_{wi}$	$S_{ew}$	20				
Area of ceiling	$S_{tr}$	21				
$S_f + S_{tr}$	$S$	44				
Reference absorption area	$A_0$	10				
Room volume	$V$	52				

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)			
			125	250	500	1000
Freefield External Noise Level	$L_{eq,ff}$	A	57	53	48	51
Simon Acoustic frame ventilator	$D_{ne,e}$		39.5	35.9	35.1	30.7
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00003	0.00006	0.00007	0.00019
Double Glazed Windows	$R_{wi}$		27	26	28	37
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00020	0.00013	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-35	-36	-37	-37
Total Absorption Area of Receiver Room	A (furnished)		13	15	17	17
	$10\log(S/A)$	G	5.3	4.7	4.1	4.1
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	29.8	25.4	18.6	21.1
						13.8
						0.5

**RESULTANT INTERNAL NOISE LEVEL** 24

Description	Term	Weighted rating	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level - Rear	$L_{max,ff}$	72dB(A)	70	68	63	70	63
Simon Acoustic frame ventilator	$D_{ne,w}$	$D_{ne,w} 33dB$	40	36	35	31	32
Glazing 6mm float / 10mm / 4mm float	$R_w$	$R_w 34dB$	27	26	28	37	36
External wall - Mansard	$R_{ew}$	$R_w 66 dB$	38	50	59	65	57
Roof	$R_{rr}$	$R_w 64 dB$	40	48	54	59	59
Total room absorption (based on RT)	$RT_{60}$	0.5	13	15	17	17	16

Derivation	Term	Value	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Facade area (including window)	$S_f$	23					
Window area	$S_{wi}$	4					
$S_f - S_{wi}$	$S_{ew}$	20					
Area of ceiling	$S_{tr}$	21					
$S_f + S_{tr}$	$S$	44					
Reference absorption area	$A_0$	10					
Room volume	$V$	52					

Description	Term from Equation	Reference letter	Octave Band Centre Frequency (Hz)				
			125	250	500	1000	2000
Freefield External Noise Level	$L_{eq,ff}$	A	70	68	63	70	63
Simon Acoustic frame ventilator	$D_{ne,e}$		39.5	35.9	35.1	30.7	32.1
	$(A_0/S)*10^{A(-D_{ne,w}/10)}$	B	0.00003	0.00006	0.00007	0.00019	0.00014
Double Glazed Windows	$R_{wi}$		27	26	28	37	36
	$(S_{wi}/S)*10^{A(-R_{wi}/10)}$	C	0.00016	0.00020	0.00013	0.00002	0.00002
External Wall Construction	$R_{ew}$		38	50	59	65	57
	$(S_{ew}/S)*10^{A(-R_{ew}/10)}$	D	0.00007	0.00000	0.00000	0.00000	0.00000
Roof Construction	$R_{rr}$		40	48	54	59	59
	$(S_{rr}/S)*10^{A(-R_{rr}/10)}$	E	0.00005	0.00001	0.00000	0.00000	0.00000
Total Sound Insulation Performance	$10\log(B+C+D+E)$	F	-35	-36	-37	-37	-38
Total Absorption Area of Receiver Room	A (furnished)		13	15	17	17	16
	$10\log(S/A)$	G	5.3	4.7	4.1	4.1	4.4
Total Internal Sound Pressure Level, Leq	Leq,2	A+F+G+3	42.9	39.7	33.3	40.4	32.2

**RESULTANT INTERNAL NOISE LEVEL** 42

## **Appendix C**



## Acoustic Performance

### Glazing Configuration

**6mm Float Glass**

10mm Cavity

**4mm Float Glass**

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### Sound Reduction Indices

Frequency, Hz / dB						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000					
27	26	28	37	36	29	34	-1	-3	29	34

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within  $\pm 2$  dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information, please consult Assumptions and Terminology section in Guardian Acoustic Assistant. By accessing this calculator, you agree not to alter or modify the generated report data and information, by any means. Any manual alteration will be your own responsibility and will annul all the content of the report.



## Acoustic Performance

### Glazing Configuration

**8mm Float Glass**

10mm Cavity

**6mm Float Glass**

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### Sound Reduction Indices

Frequency, Hz / dB*						Rw	C	Ctr	OITC	STC
125	250	500	1000	2000	4000	35	-1	-3	31	35
30	27	29	38	35	35					

\*The values expressed in the frequency table correspond to the central values of the 1/3 octave band

Disclaimer: The acoustic performance data provided in the reports is based on a test protocol or an estimation and may be used if user actual glazing is identical to input data described herein. Acoustic performance data herein is only applicable for glazing dimensions 1,23 m x 1,48 m (as per testing standard). Estimation of acoustic performance is based on component-similarity assumptions which are derived from measured data and interpolation to expand the database of values from test protocols. Due to inherent variations in acoustic performance when testing in accordance with EN ISO 10140-3/EN ISO 10140-2, some variation in the calculated performance can also be expected. As such, the weighted performance, Rw, and adaptation terms, C and Ctr, should typically be considered to be accurate within  $\pm 2$  dB. However, wider deviations can occur. Actual performance may vary according to the glazing dimensions, frame system, noise sources and many other parameters. The acoustic performance data herein should not be used as a substitute for tests of actual glazing. For more information, please consult Assumptions and Terminology section in Guardian Acoustic Assistant. By accessing this calculator, you agree not to alter or modify the generated report data and information, by any means. Any manual alteration will be your own responsibility and will annul all the content of the report.

# MA3051

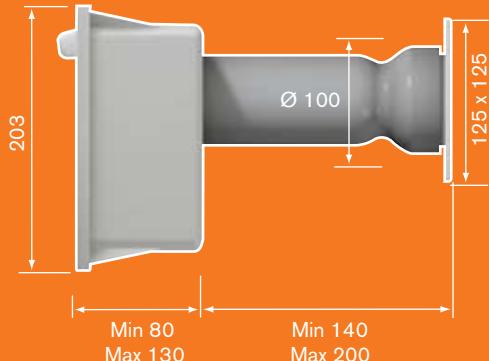
## Acoustic wall ventilator

### Physical specification

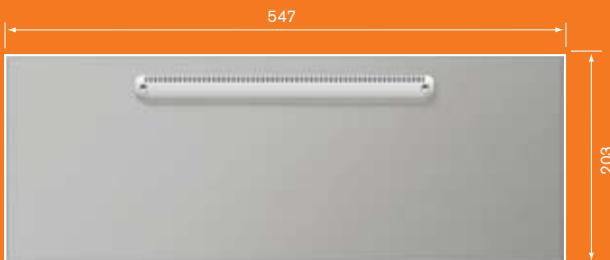
All measurements in millimetres.



External grille



Side



Internal

**Weight:** 2.655 kg

**Materials:** PVC: Casing for wall vent, duct, external grille and internal ventilator. Acoustic lining and material inside wall vent.

### Features

- Acoustic background ventilator
- Provides acoustic attenuation to Dn,e w 55dB
- 2500mm<sup>2</sup> equivalent area performance
- Suitable for external wall thicknesses of 140mm and above
- Internal wall constructions of between 100mm and 150mm
- Supplied with internal controllable vent and white/sand external grilles
- Conforms to acoustic requirements of Noise Insulation Regulations 1975, one of only a small number of products available in the UK

### Controls

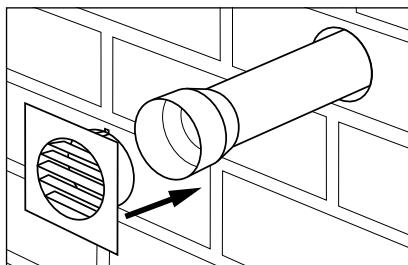
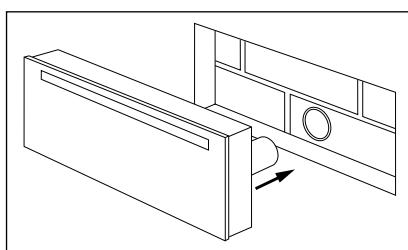
Model	Operation
MA3051	Internal controllable trickle ventilator

### Installation

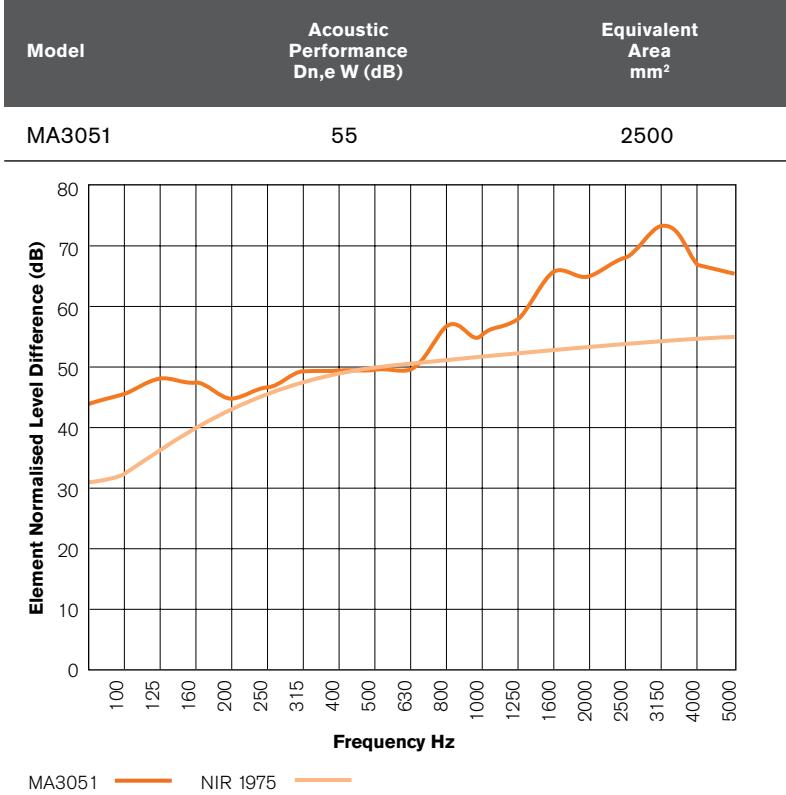
Instructions are provided with product including wall template for cut out.

Bonding compound is required to complete installation.

Protective strip protect internal unit until decoration is complete within dwelling.



## Performance



Frequency	100	125	160	200	250	315	400	500
dB	45	48	47	44	46	49	49	49

Frequency	630	800	1000	1250	1600	2000	2500	3150
dB	49	56	54	57	66	65	68	66

D<sub>n,e,w</sub> (C;Ctr) = 55(-1;-3) dB

C: Pink Noise

Ctr: Road Noise

## Specification



## Considering noise and domestic ventilation together

If life was simple then noise issues would be simply dealt with by swapping standard products for acoustic products.

In some circumstances, this may be achievable, however the nature of acoustic products means that they are generally larger and more bulky and multiple installations, (to achieve higher ventilation rates) of the same product can also effect acoustic performance.

With this in mind, noise and ventilation must be considered together at design. Whole house systems that have limited penetrations in the facade of a building often work well, however a whole range of individual products such as airbricks and wall ventilators are available with db reductions of up to 55.

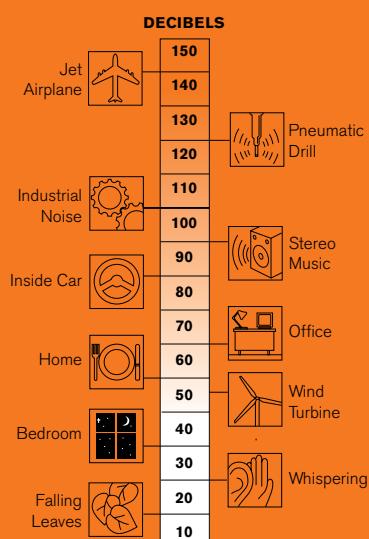
The best thing to do is ask – too many times have buildings been built and then acoustic ventilation been thought about, thus reducing options and sometimes meaning costly re-works on site.

## Measuring sound

Sound can be measured in two ways:

- Intensity/Loudness of sound is measured in decibels – dB
- Pitch of sound is measured in frequency of vibrations per second

The decibel scale runs from the faintest sound the human ear can detect (0dB) to over 180dB that is similar to the noise a rocket creates during a launch.



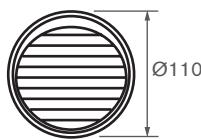
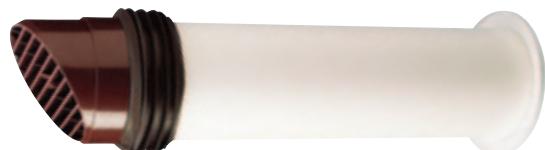
# AWV39

Acoustic wall ventilator

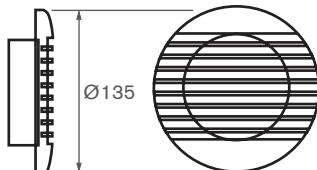
## Physical specification

All measurements in millimetres

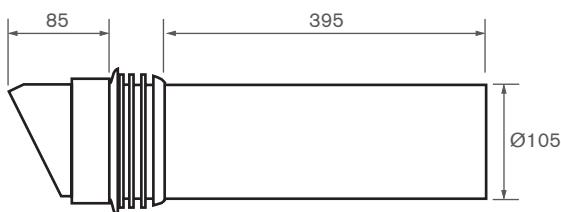
**Weight:** 0.7440kg  
**Materials:** PVC



**External grille (supplied separately)**



**Internal**



**Side**

## Features and benefits

Designed for use in refurbishment applications.

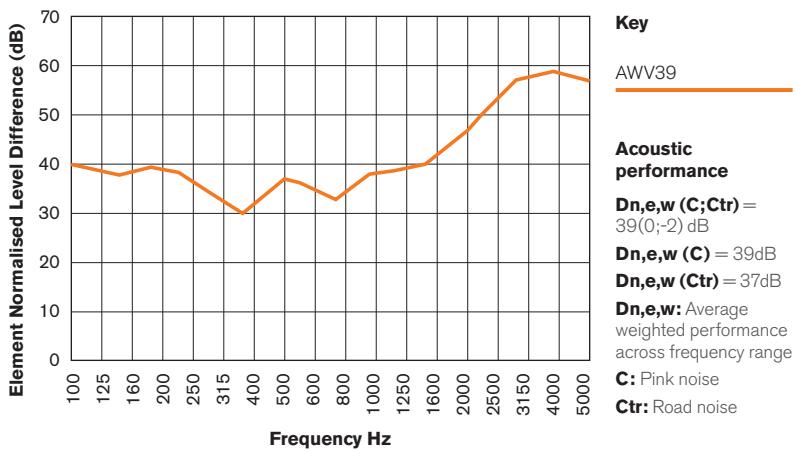
Provides acoustic attenuation to Dn,e,w 39dB.

2500mm<sup>2</sup> equivalent area performance.

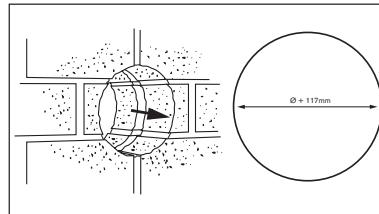
Suitable for wall thicknesses 255–370mm.

## Performance

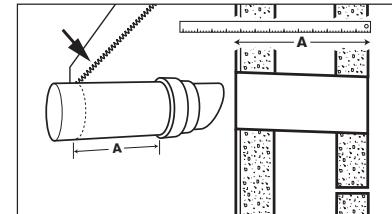
Model	Acoustic performance Dn,e,w (dB)	Equivalent area mm <sup>2</sup>
AWV39	39	2500



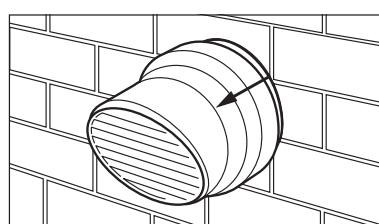
## Installation



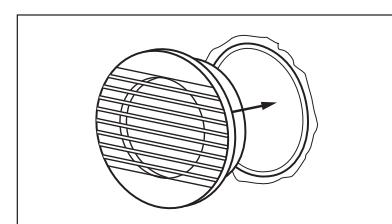
Using a 117mm core drill, cut a hole through wall



Measure wall thickness and cut down plastic sleeve as required



Push the sleeve through the wall. The seal will automatically sit between the sleeve and the external grille, providing a watertight fit



Push fit internal grille

# Simon

**Acoustic Solutions** - Simons have launched a range of acoustic ventilators to assist clients in creating a satisfactory solution for all their acoustic requirements. All ventilators in the range meet the requirements of Document F and Document E of the Building Regulations

# Simon Acoustic Ventilators

## Specification

- Sound reduction of up to 41dB
- All models have been independently tested in accordance with BS EN ISO 717-1:1997 (airborne sound insulation & BS EN 20140-10:1992)
- Acoustic canopy available in any standard RAL colour and silver anodised finish
- Available in 5 internal options
- All options can be supplied on carrier bar
- Some models available with humidity control
- All models have a minimum Equivalent Area of 2,500mm<sup>2</sup>
- Meets World Health Organisation recommended reduction of 33dB



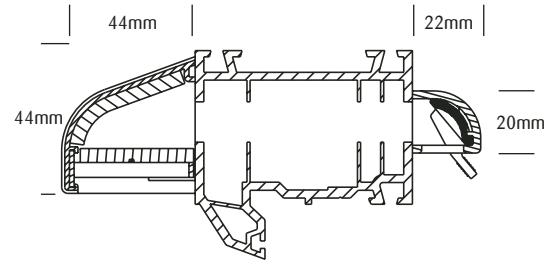
**Simon**  
Air Management  
Systems

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Tel: 01805 623721 Fax: 01805 624578 E-mail: [info@rwsimon.co.uk](mailto:info@rwsimon.co.uk)

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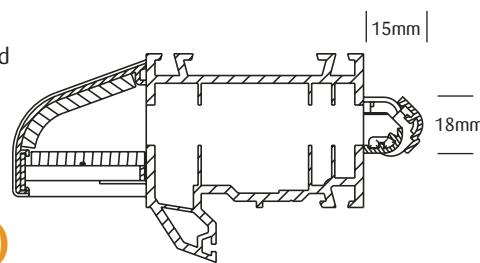
## Simon Acoustic FV ( Framevent )

- Supplied with a PVCu internal flap unit and aluminium external canopy
- 4080<sup>mm<sup>2</sup></sup> measured area 2500<sup>mm<sup>2</sup></sup> Equivalent Area
- Available with white, bright white, mahogany & tan internals and any standard RAL colour or anodised external aluminium canopy
- Achieves sound reduction of 40dB closed and 33dB open
- Rod options available



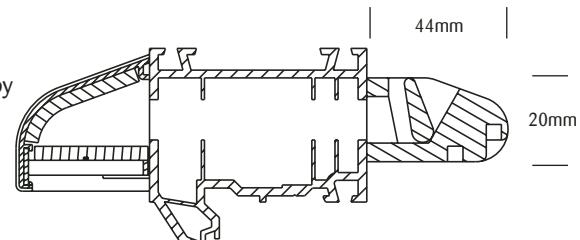
## Simon Acoustic SL ( Slimline )

- Manufactured fully from aluminium. Available in any standard RAL colour, or anodised internal and externals
- 4080<sup>mm<sup>2</sup></sup> measured area 2,500<sup>mm<sup>2</sup></sup> Equivalent Area
- Achieves sound reduction of 39dB closed and 33dB open
- Rod options available



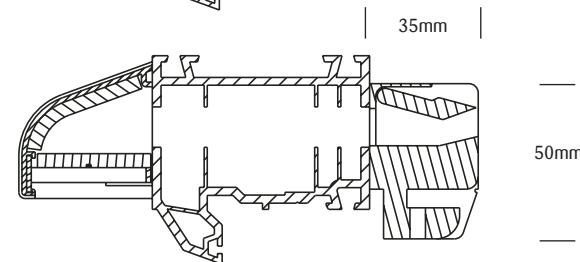
## Simon Acoustic EMM ( Humidity Controlled )

- Internal unit and an aluminium external canopy
- Achieves 2500<sup>mm<sup>2</sup></sup> Equivalent Area
- Available in white internally and any standard RAL colour or anodised external canopy
- Uses a hygrometric sensor which opens and closes the flap dependent on the amount of moisture in the room
- Achieves sound reduction of 39dB closed and 33dB open



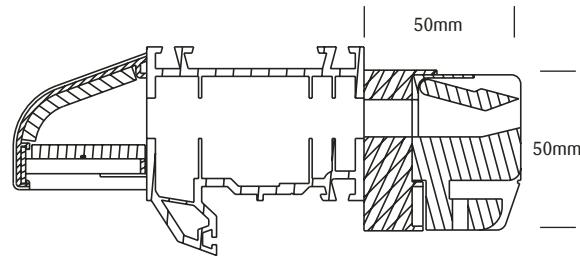
## Simon Acoustic EHA

- Internal automatic opening unit and aluminium external canopy
- Achieves a minimum Equivalent Area of 2500<sup>mm<sup>2</sup></sup>
- Available in white internally and any standard RAL colour or anodised external
- Uses a hygrometric sensor which opens and closes the flap dependent on the amount of moisture in the room
- Achieves sound reduction of 38dB closed and 36dB open



## Simon Acoustic EHAS

- Internal automatic opening unit and aluminium external canopy
- Has a minimum Equivalent Area of 2500<sup>mm<sup>2</sup></sup>
- Available in white internally and any standard RAL polyester powder coated finish or anodised external canopy
- Uses a hygrometric sensor which opens and closes the flap dependent on the amount of moisture in the room.
- Includes additional acoustic sleeve to increase the acoustic properties
- Achieves sound reduction of 41dB closed and 38dB open



## Specifications

	dB Closed	dB open	EA to BS 13141-1	Measured Area mm <sup>2</sup>	Dimensions Int.	Dimensions Ext	Slot size
Simon Acoustic FV	40	33	2830	4080	400 x 20	431 x 45	340 x 12
Simon Acoustic SL	39	33	2967	4080	375 x 18	431 x 45	340 x 12
Simon Acoustic EMM	39	33	3199	4080	420 x 30	431 x 45	340 x 12
Simon Acoustic EHA	38	36	2799	4080	420 x 50	431 x 45	340 x 12
Simon Acoustic EHAS	41	38	2799	4080	420 x 50	431 x 45	340 x 12

### Internal Colour Options

Simon Acoustic FV White, Brown and Tan  
 Simon Acoustic SL Any RAL colour and silver anodised  
 Simon Acoustic EMM White only  
 Simon Acoustic EHA White only  
 Simon Acoustic EHAS White only

All the above acoustic vents can be supplied on glazed in carrier bar.

By adding additional units the acoustic performance may be reduced.

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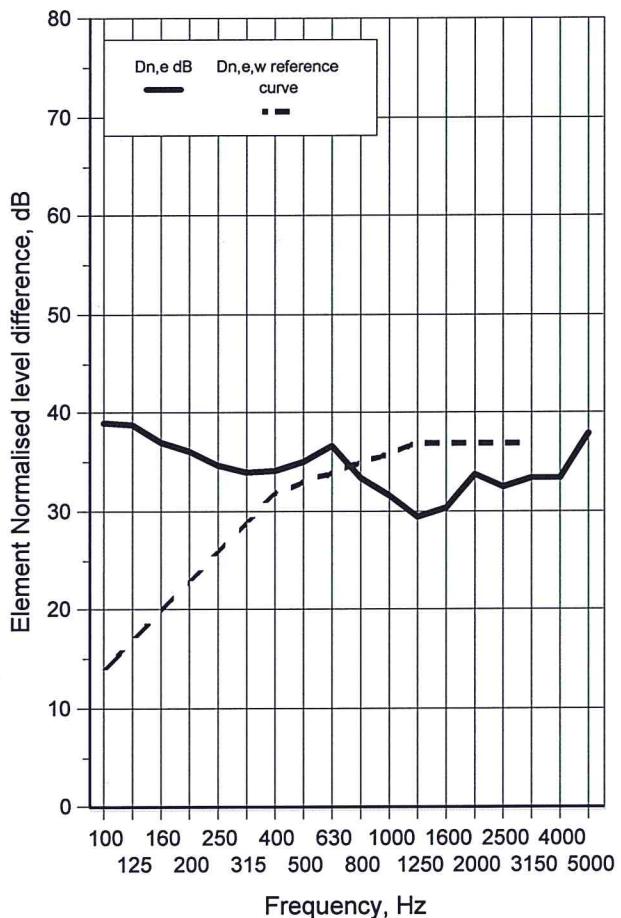


**Simon**  
**Air Management**  
**Systems**

## Data Sheet 10

Test Number: 12 Air temperature: 15.9 °C  
 Test Date: 16/01/2007 Air humidity: 61 %  
 Number of items tested at once: 1 Receiving room volume: 300 m<sup>3</sup>  
 Nominal free area of single ventilator: 2500 mm<sup>2</sup> Source room volume: 115 m<sup>3</sup>  
 Product identification: Simon Acoustic TTF Slimline - Open

Freq f Hz	Element normalised level difference		
	Dn,e dB	1/3 Oct	1/1 Oct
100	39.0	\$	
125	38.9	\$	38.2
160	37.0	%	
200	36.1	%	
250	34.7	%	34.8
315	33.9		
400	34.1		
500	35.1		35.2
630	36.7		
800	33.4		
1000	31.7		31.2
1250	29.4		
1600	30.3		
2000	33.7		31.9
2500	32.5		
3150	33.5		
4000	33.5		34.5
5000	37.9		
6300+	39.6		
8000+	39.4		39.9
10000+	40.7		
Average			
100-3150	34.4		



Rating according to BS EN ISO 717-1:1997

Dn,e,w(C;Ctr)= 33 (-1;-1) dB

Notes :\* designates measurement corrected for background

# designates limit of measurement due to background

% designates measurement corrected for flanking

\$ designates limit of measurement due to flanking

+ designates frequency beyond standard

v1.2