# 163 FIELD END ROAD LONDON HA5 1QL

## BS4142 PLANT NOISE ASSESSMENT

**24 November 2025**

**Jasmine Lounge**

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## BS4142 PLANT NOISE ASSESSMENT

**Document Reference: RP.251124.0 - 163 FIELD END ROAD LONDON - PLANT NOISE ASSESSMENT.DOCX**

| Revision | Description | Issued by | Issue date |
|---|---|---|---|
| - | First Issue – Plant Noise Assessment | Damien Hesnan | 24/11/2025 |
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## 1.0 INTRODUCTION

Aran Acoustics in collaboration with Airtight Building Solutions Ltd have been appointed to carry out a noise impact assessment for the proposed installation of a kitchen extract system at 163 Field End Road, London.

A noise survey and assessment has been requested to ensure that noise emissions from the proposed plant do not cause undue disturbance to nearby noise sensitive locations.

The purpose of this assessment is to determine the existing noise levels at the nearest noise sensitive location and establish the maximum permissible noise levels from the plant.

To establish suitable plant noise levels, an assessment has been carried out in accordance with BS 4142:2014 'Methods for rating and assessing industrial and commercial sound'. This assessment has been benchmarked against an environmental noise survey undertaken on 19 November 2025.

This report therefore describes the noise survey and its results. Figure 4.1 contains a graphical representation of the noise measurements taken on site. Section 5.0 provides the maximum permissible noise levels for the proposed plant. Section 6.0 presents an assessment of plant noise levels based on the proposed installation and its location.

## 2.0 SITE DESCRIPTION

The site is located at 163 Field End Road, London, forming part of a parade of mixed-use commercial premises fronting Field End Road. The premises comprise a ground floor commercial unit with residential accommodation situated on upper floor levels.

Proposals include the installation of a kitchen extract system serving the ground floor unit. The extract fan and associated ductwork are to be installed externally at roof level to the rear of the property, with the discharge directed horizontally as shown on the drawings included in Appendix A.

The nearest noise sensitive receptor is the first floor residential window situated directly above the host premises. Additional residential properties are located to the rear of the site; however, the dominant assessment location is the first floor window immediately overlooking the proposed plant installation.

The existing acoustic environment is characterised by continuous road traffic activity along Field End Road, together with noise associated with parking movements, commercial activity from the surrounding units and existing mechanical plant installed on nearby premises. These noise sources contribute to the residual acoustic climate across both daytime and evening periods.

Figure 2.1 below shows a location map and aerial photo of the site and surrounding area.

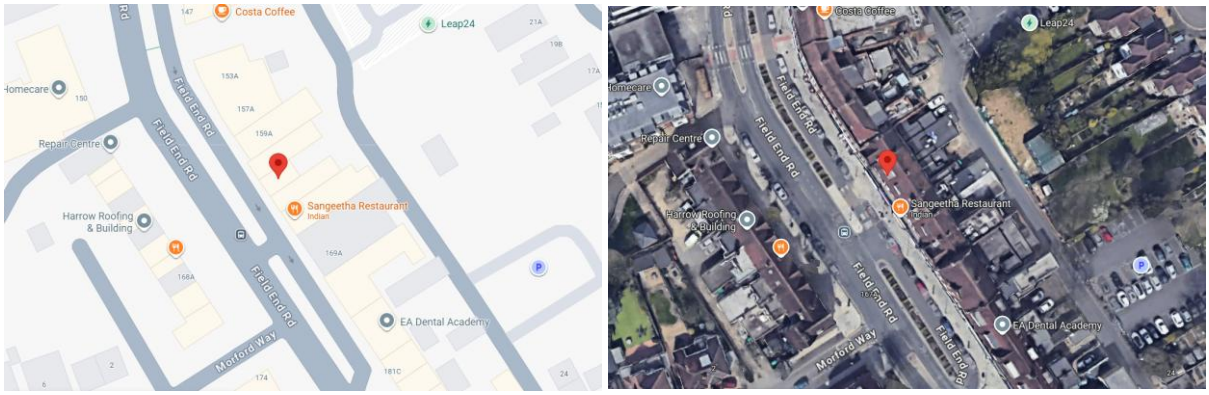



***Table 2.1 – Location map and aerial photo of the site****

**Imagery courtesy of Google Maps*

## 3.0 ENVIRONMENTAL NOISE SURVEY

An environmental noise survey was carried out at the site on 19 November 2025. The survey was carried out over a continuous 24-hour period to capture both daytime and night-time acoustic conditions representative of the surrounding environment.

The microphone was mounted at first floor height at the rear of the premises in close proximity to the nearest residential window. The position was selected to be representative of the most exposed façade of the host property in relation to the proposed plant installation.

A site plan showing the microphone location is provided in Appendix A. Site photos of the microphone position are provided in Appendix B.

### 3.1 Measurement Equipment

The following measurement equipment was used, which complies with the performance specifications for a Class 1 device in accordance with BS EN 61672-1, BS EN 61260 and BS EN 60942.

| Name | Serial Number | Last Calibrated | Calibration Due |
|---|---|---|---|
| **Norsonic Precision Sound Analyser Type 140** | 1404768 | Dec 2024 | Dec 2026 |
| **Norsonic Type 1209 Pre-amplifier** | 31313 | Dec 2024 | Dec 2026 |
| **Norsonic Type 1225 Microphone** | 157320 | Dec 2024 | Dec 2026 |
| **Rion Type NC-74 Acoustic Calibrator** | 35046846 | Feb 2025 | Feb 2026 |

***Table 3.1 – Measurement equipment used on site***

Measurements were logged as consecutive A weighted 15-minute samples with statistical indices stored for each interval. The sound level meter was field calibrated immediately before and after the survey with no material drift observed.

### 3.2 Weather Conditions

The weather was mainly fine and dry for the duration of the survey. Wind speed remained below 5 m/s. The temperature was approximately 01 - 14 $^{o}$C.

The weather conditions were seen as suitable for environmental noise surveying in accordance with BS 7445-1:2003 '*Description and measurement of environmental noise*'.

## 4.0 SURVEY RESULTS

The noise levels measured during the survey period are shown in Figure 4.1 below. The full set of acoustic data measured on site is available upon request.

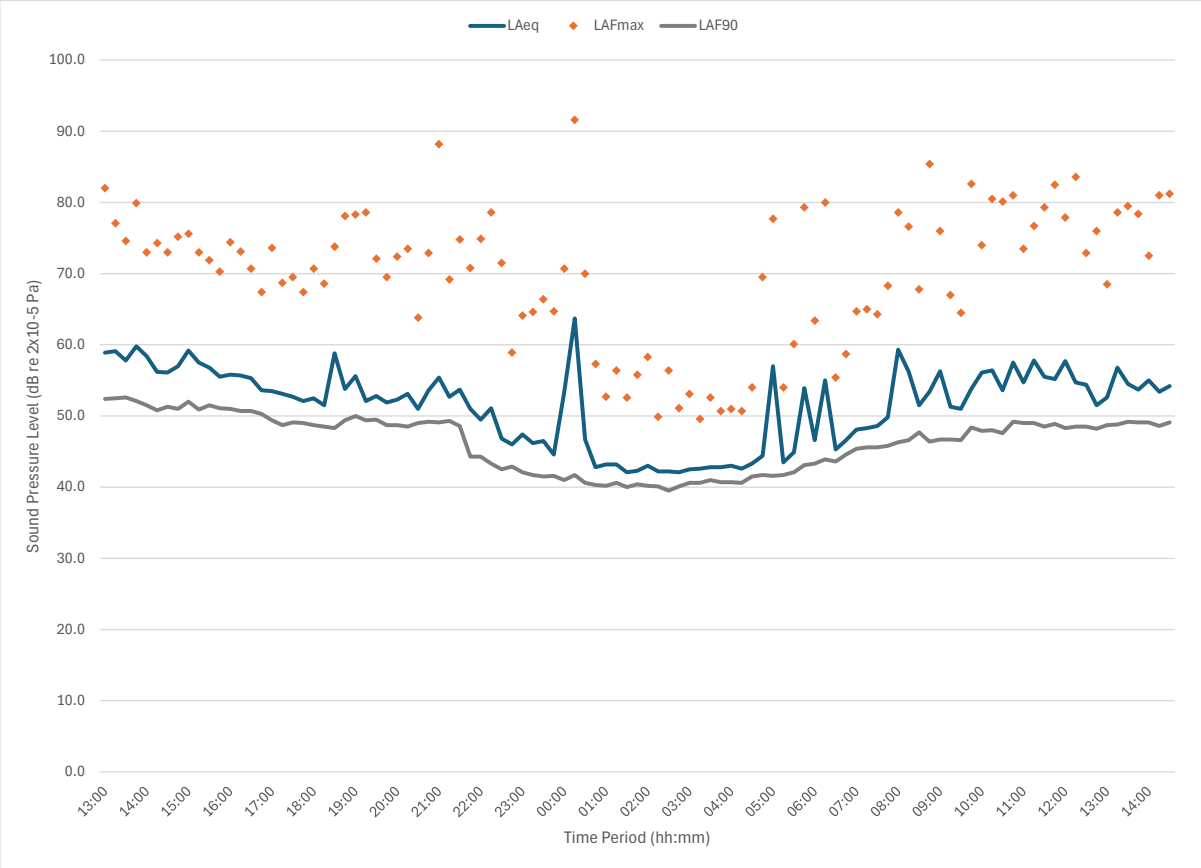



***Figure 4.1 – Measured noise levels***

Results of the survey show that noise levels to the rear of the property remained relatively consistent through the day with a reduction during the night period. This is attributable to road traffic and existing plant activity in the locality.

The following table provides a summary of the noise levels measured on site at the fixed microphone position during the survey period including the equivalent continuous A-weighted sound pressure level; $L_{Aeq,T}$ and representative background noise level; $L_{A90,T}$.

| Time Period | Average Noise Level $L_{Aeq}$, dB | Representative Background $L_{A90}$, dB |
|---|---|---|
| **Day (07:00 – 23:00 hours)** | 55 | 49 |
| **Night (23:00 – 07:00 hours)** | 51 | 41 |

***Table 4.1 - Summary of measured noise levels***

## 5.0 ASSESSMENT CRITERIA

Section 4.0 above provides a summary of measured noise levels on site. The following section provides a summary of guidance documentation relevant to this development.

### 5.1 British Standard 4142

BS 4142:2014 describes a method of determining the level of noise of an industrial nature, together with the procedures for assessing whether the noise in question is likely to give rise to complaints from persons living in the vicinity. As such, an assessment to BS 4142 is typically called for within planning conditions.

The likelihood of complaints in response to a specific noise depends on various factors. BS 4142 assesses the likelihood of complaints by considering the margin by which the noise in question exceeds the background noise level. BS 4142 states that:

a) Typically, the greater this difference, the greater the magnitude of the impact.
b) A difference of around +10 dB or more is likely to be an indication of a significant adverse impact, depending on the context.
c) A difference of around +5 dB is likely to be an indication of an adverse impact, depending on the context.
d) The lower the rating level is relative to the measured background sound level, the less likely it is that the specific sound source will have an adverse impact or a significant adverse impact. Where the rating level does not exceed the background sound level, this is an indication of the specific sound source having a low impact, depending on the context.

This standard also allows for an appropriate correction for the acoustic features present in the noise using a number of methods. A correction should be applied if one or more of the following features (see the list below), are present within the noise sources in question.

- The noise is of a tonal nature, i.e. it contains a distinguishable, discreet, continuous note such as whine, hiss, screech, hum;
- The noise is impulsive, i.e. it contains distinct impulses such as bangs, clicks, clatters, or thumps;
- The noise contains other characteristics that are neither tonal nor impulsive but is irregular enough to attract attention.

It can be concluded from BS4142 guidance document that noise levels from plant and equipment associated with the development should not generally exceed the background noise level when measured at the nearest noise sensitive location. This is a positive indication of low noise impact.

## 5.2 Target Plant Noise Levels

The proposed operating hours for the kitchen extract system are between 10:00 and 23:00 hours. The representative background sound level measured during the survey was 49 dB $L_{A90}$ during the daytime period and 41 dB $L_{A90}$ during the night-time period. Although the system is not intended to operate beyond 23:00 hours, the night-time background level has been included for completeness.

The manufacturer's octave-band sound power data and the calculated spectrum at the receptor have been reviewed. The predicted plant noise is broadband in character with no tonal, impulsive or other distinguishing acoustic features. On this basis no acoustic feature correction is applied in accordance with the procedures set out in BS 4142.

The design aim is for the rating level from the plant to be at least 10 dB below the representative background sound level at the nearest residential receptor. Based on the measured background levels, the maximum permissible specific sound levels at the nearby receptors are given in Table 5.1.

| Time Period | Representative Background, $L_{A90}$ | Tolerance Factor | Correction Factor | Max Noise Level at Residential |
|---|---|---|---|---|
| **Day (07:00 – 23:00 hours)** | 49 dBA | -10 dB | 0 dB | **39 dBA** |
| **Night (23:00 – 07:00 hours)*** | 41 dBA | -10 dB | 0 dB | **31 dBA** |

***Table 5.1 - Plant noise level targets***

*The extract system is not currently proposed to operate at night. The night-time target is included for completeness.

## 6.0 PLANT NOISE LEVEL ASSESSMENT

Noise predictions have been undertaken for the proposed kitchen extract system using the octave band sound power data provided for the Helios GBW 500/4/4 extract fan. The assessment includes contributions from inlet duct breakout incorporating a CP03-C-0560-1D attenuator, fan case breakout, and the outlet discharge fitted with a CP03-C-0560-2D attenuator. The fan and ductwork assembly are to be installed at roof level to the rear of the premises with a horizontal discharge, as indicated on the drawings provided in Appendix A.

Predicted specific sound levels at the nearest first floor residential receptor have been calculated using standard propagation methods, including silencer insertion loss, breakout attenuation through 0.55mm galvanised steel ductwork, end reflection, and distance attenuation from each component. The receptor is located at the first floor rear window directly above the host premises.

The combined level from all elements of the kitchen extract system has been calculated as **32dBA** at the nearest noise sensitive receptor. This is comfortably below the maximum permissible rating level of **39dBA** derived in Section 5.2 and therefore meets the design target required to achieve a low impact in accordance with BS 4142.

The octave band calculation results are presented in Table 6.1 below.

| | Octave Band Centre Frequency, dB | | | | | | | |
|---|---|---|---|---|---|---|---|---|
| **Noise Source** | **63 Hz** | **125 Hz** | **250 Hz** | **500 Hz** | **1.0 K Hz** | **2.0 K Hz** | **4.0 K Hz** | **dBA** |
| **Inlet Duct** | -33.7 | 15.3 | 17.3 | 7.3 | 7.3 | 2.3 | -8.7 | **13** |
| **Fan Case Breakout** | -32.9 | 31.1 | 31.1 | 15.1 | 17.1 | 13.1 | 10.1 | **25** |
| **Duct Outlet** | -45.1 | 17.9 | 28.9 | 22.2 | 21.1 | 26.1 | 24.1 | **31** |
| **Combined SPL (Lp)** | -30.1 | 31.4 | 33.3 | 23.1 | 22.7 | 26.4 | 24.3 | **32** |

***Table 6.1 – Calculated Plant Noise Levels***

The calculated rating level is therefore 7 dB below the daytime design criterion of 39 dBA. On this basis, the plant noise emissions are not expected to give rise to adverse impact at nearby residential receptors under the proposed operating hours.

Plant noise calculation sheets are provided in Appendix C. Manufacturers noise level data sheets are provided in Appendix D.

## 6.1 Mitigation Strategy

The following mitigation measures are integral to the extract system design and have been included within the plant noise calculations presented in Section 6.0.

A CP03-C-0560-1D silencer is installed on the inlet side of the fan to reduce upstream breakout from the external ductwork. A CP03-C-0560-2D silencer is installed on the discharge side to control noise emitted from the horizontal outlet located on the roof of the proposed ground floor extension. Both silencers have been selected based on their octave band insertion loss characteristics, which have been applied directly within the assessment.

The external ductwork is constructed from 0.55mm galvanised steel, which provides inherent attenuation through breakout surfaces and contributes to the overall sound reduction performance of the system. No additional casing lagging or secondary enclosure is proposed or required based on the calculated sound levels.

These measures ensure that noise emissions from the extract system comply with the derived daytime planning target at nearby residential windows.

## 6.2 Vibration

Mechanical plant such as extract fans can transmit structure-borne vibration into the building fabric, which may re-radiate as audible noise. In this case, the extract fan and associated ductwork will be mounted on the flat roof of the proposed ground floor extension, with the discharge facing away from the host building towards the rear service yard.

The roof-mounted configuration provides natural separation between the fan assembly and the first floor residential accommodation above the premises. Standard installation practice requires the fan unit to be mounted on suitable anti-vibration pads with flexible connectors fitted at both the inlet and outlet to prevent rigid coupling to the ductwork system. These measures limit the potential for vibration transfer into the supporting structure.

The horizontal steel ductwork will be supported from the new extension roof structure. Provided that intermediate supports incorporate suitable resilient packers or rubber isolation where required, the risk of vibration transmission into the main building fabric is minimal. No direct fixing of the system to internal partitions or upper floor structures is proposed.

With these provisions in place, the likelihood of structure-borne vibration or re-radiated noise affecting nearby residential rooms is considered negligible. The proposed installation is therefore expected to operate without giving rise to vibration-related disturbance.

## 7.0 SUMMARY AND CONCLUSION

A noise impact assessment has been undertaken for the proposed kitchen extract system to be installed at 163 Field End Road, London. The system comprises a Helios GBW 500/4/4 extract fan installed at roof level to the rear of the premises, with associated inlet and outlet ductwork fitted with CP03-C-0560 silencers. The installation serves the ground floor commercial unit and operates between 10:00 and 23:00 hours.

A 24-hour environmental noise survey was carried out on 19 November 2025 to establish representative background sound levels at the nearest noise sensitive receptor, identified as the first floor rear-facing residential window above the host premises. The measured background sound level was 49 dB $L_{A90}$ during daytime hours and 41 dB $L_{A90}$ during night-time hours.

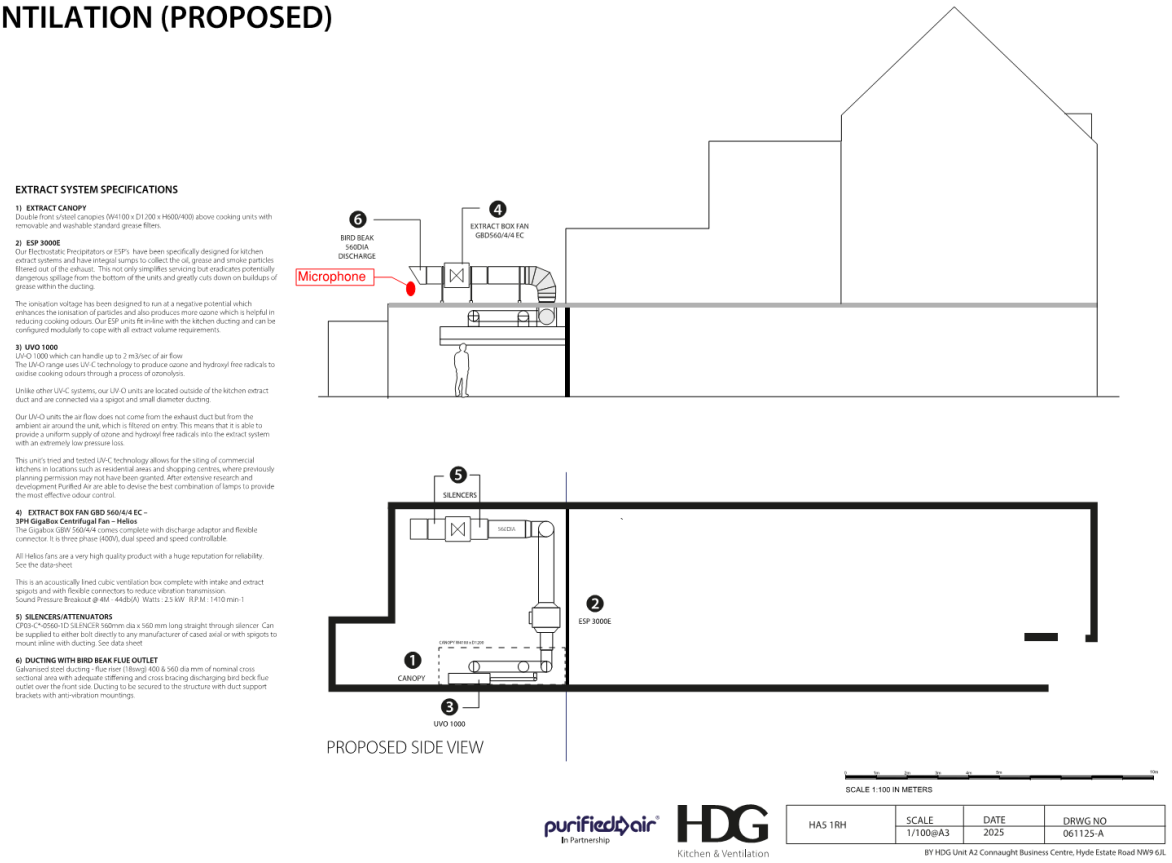
Based on BS 4142 guidance, a design target of 39 dBA was derived for the maximum specific sound level from the proposed plant at the nearest receptor. This target corresponds to the background sound level minus 10 dB to ensure a low impact, with no acoustic feature correction applied owing to the broadband and non-tonal nature of the predicted plant noise.

Octave band calculations have been undertaken for the inlet duct breakout, fan case breakout and the outlet discharge incorporating the specified silencers, breakout attenuation and propagation to the receptor. The combined specific sound level at the most exposed residential façade is calculated to be 32 dBA, which is 7 dB below the daytime design target.

The assessment therefore confirms that the proposed kitchen extract system meets the BS 4142 design criteria and is not expected to result in adverse impact at nearby residential properties. With the silencers and installation configuration included within the design, the system is considered suitable for operation during the proposed hours without causing disturbance.

## APPENDIX A – SITE PLAN

## VENTILATION (PROPOSED)



## APPENDIX B – SITE PHOTOS

## APPENDIX C – PLANT NOISE CALCULATION SHEET

| Kitchen Extract Inlet Duct | QTY | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1.0 kHz | 2.0 kHz | 4.0 kHz | dBA |
|---|---|---|---|---|---|---|---|---|---|
| **Helios GBW 500/4/4 (Lw)** | 1 | | 57 | 66 | 69 | 74 | 70 | 64 | **63** |
| CP03-C-0560-1D Attenuator | 1 | -2 | -4 | -7 | -14 | -14 | -9 | -9 | |
| 0.55mm Galvanised Steel Duct SRI | | 0.0 | -6.0 | -10.0 | -16.0 | -21.0 | -27.0 | -32.0 | |
| Distance Attenuation | 10.9 | -31.7 | -31.7 | -31.7 | -31.7 | -31.7 | -31.7 | -31.7 | |
| **SPL at Receiver (Lp)** | | -33.7 | 15.3 | 17.3 | 7.3 | 7.3 | 2.3 | -8.7 | **13** |

| Kitchen Extract Case Breakout | QTY | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1.0 kHz | 2.0 kHz | 4.0 kHz | dBA |
|---|---|---|---|---|---|---|---|---|---|
| **Helios GBW 500/4/4 (Lw)** | 1 | 0 | 64 | 64 | 48 | 50 | 46 | 43 | **43** |
| SuperLag Superflex Prime 5/25 | 1 | | | | | | | | |
| Barrier Correction | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| Distance Attenuation | 12.4 | -32.9 | -32.9 | -32.9 | -32.9 | -32.9 | -32.9 | -32.9 | |
| **SPL at Receiver (Lp)** | | -32.9 | 31.1 | 31.1 | 15.1 | 17.1 | 13.1 | 10.1 | **25** |

| Kitchen Extract Duct Outlet | QTY | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1.0 kHz | 2.0 kHz | 4.0 kHz | dBA |
|---|---|---|---|---|---|---|---|---|---|
| **Helios GBW 500/4/4 (Lw)** | 1 | | 62 | 74 | 75 | 75 | 74 | 70 | |
| CP03-C-0560-2D Attenuator | 1 | -3 | -6 | -10 | -19 | -20 | -14 | -12 | |
| Duct Attenuation | 0.5 | -0.4 | -0.4 | -0.4 | -0.1 | -0.1 | -0.1 | -0.1 | |
| Bend Losses | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | |
| End Reflection Loss | 450 | -8 | -4 | -1 | 0 | 0 | 0 | 0 | |
| Distance Attenuation | 13.8 | -33.8 | -33.8 | -33.8 | -33.8 | -33.8 | -33.8 | -33.8 | |
| **SPL at Receiver (Lp)** | | -45.1 | 17.9 | 28.9 | 22.2 | 21.1 | 26.1 | 24.1 | **31** |

| **Combined SPL at Receiver (Lp)** | | -30.1 | 31.4 | 33.3 | 23.1 | 22.7 | 26.4 | 24.3 | **32** |
|---|---|---|---|---|---|---|---|---|---|

## APPENDIX D – TECHNICAL DATA SHEETS

# 560 mm ø GigaBox centrifugal fan

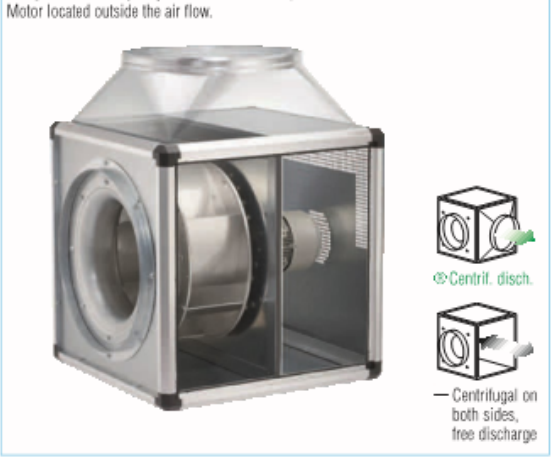
Helios

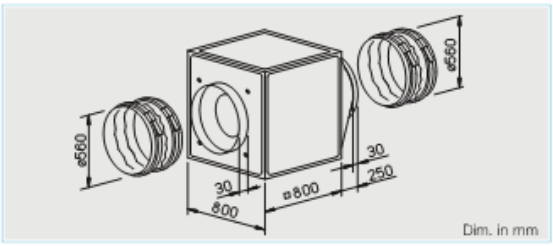
**GB**

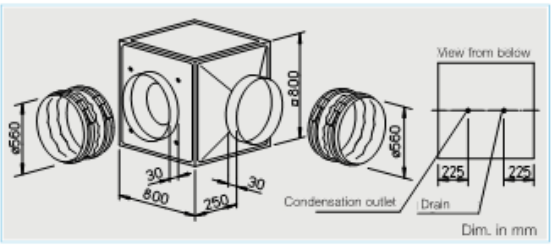
Arbitrary installation position and flexible assembly by five possible discharge directions.


**GB T120**

Designed for moving dirty, humid and hot air up to max. 120° C.
Motor located outside the air flow.




■ **Special features of types GB T120**
- Designed for moving dirty, humid and hot air volumes up to max. 120° C.
- Motor located outside of air flow.
- Temperature insulated partition panel between motor and impeller, lined with 20 mm thick, flame-retardant mineral wool.
- Easily accessible motor and impeller unit, removable without disassembling the system components.
- Inspection cover with handle, simply remove for cleaning and maintenance.
- Condensate collector with condensate spigot included in delivery. Drill hole for rain drainage (accessories) for outdoor installation is prepared.

□ **Assembly GB T120**
Installation must be carried out with condensation discharge showing downward. Flexible assembly by three possible centrifugal discharge directions via the discharge adapter.
Outdoor installation is possible using outdoor cover hood and external weather louvers (accessories).

■ **Feature**

□ **Assembly of types GB**
Arbitrary installation position and flexible assembly by five possible discharge directions via the discharge adapter.
For wall mounting the wall bracket (accessories) have to be used. Outdoor installation is possible using outdoor cover hood and external weather louvers (accessories).

■ **Specification of both types**

□ **Casing**
Self-supporting frame construction from aluminium hollow profiles. Double-walled side panels from galvanised sheet steel, lined with 20 mm thick temperature insulating and flame-retardant mineral wool. Intake cone for ideal inflow as well as spigot and flexible sleeve (for the respective max. permissible air flow temperature) for duct connection. With discharge adapter (from square to circular) on the pressure side for low-loss discharge and flexible sleeve to reduce vibration transmission. Simple positioning by standard crane hooks.

□ **Impeller**
Smooth running backward curved aluminium centrifugal impeller highly efficient and direct driven. Energy efficient with a low noise development. Dynamically balanced together with the motor to DIN ISO 1940 Pt.1 – class 6.3.

□ **Motor**
Maintenance-free external rotor motor or IEC-standard motor protected to IP 54. With ball bearings and interference-free as standard.

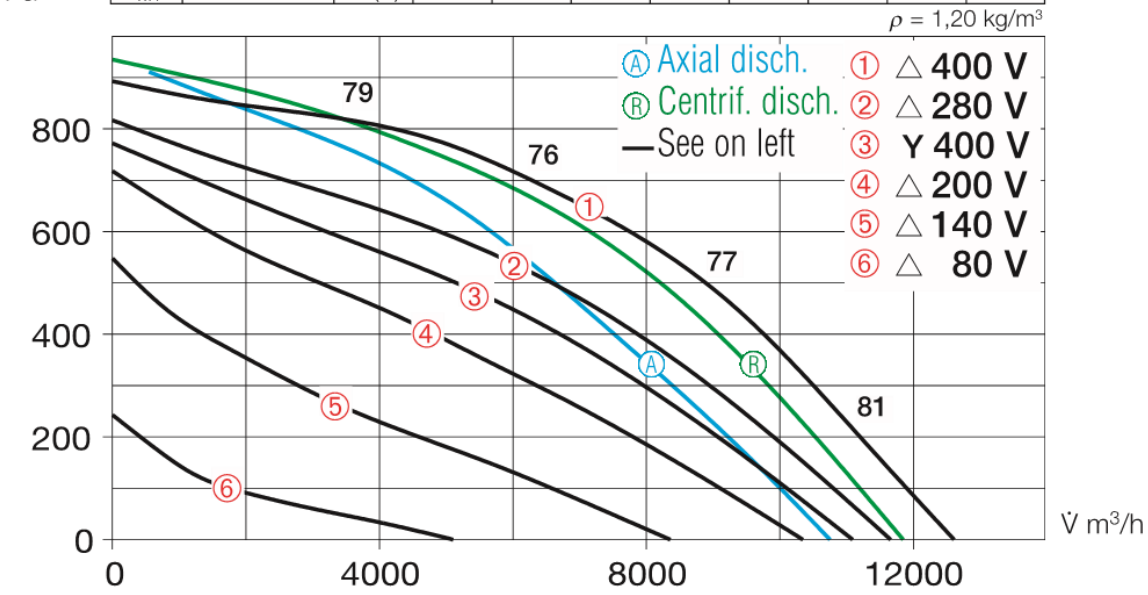
□ **Electrical connection**
Standard terminal box (IP 54) fitted on the motor; with GB T120 fitted on the motor support plate.

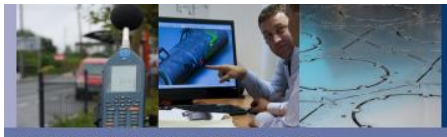
| Type | Ref. no. | Air flow volume (FID) | R.P.M. | Sound press. case breakout | Motor power (nominal) | Current Full load | Current speed controlled | Wiring diagram | Maximum air flow temperature Full load | Maximum air flow temperature controlled | Weight (net) kg | 5 step transformer controller with mot. protect. unit Type | Ref. no. | 5 step transformer controller without mot. protect. unit Type | Ref. no. | Full motor protection unit using the thermal contacts Type | Ref. no. |
|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|---|
| | | V m³/h | min⁻¹ | dB(A) in 4 m | kW | A | A | No. | +°C | +°C | kg | | | | | | |
| **1 Phase motor, 230 V / 1 ph. / 50 Hz, capacitor motor, protection to IP 54** | | | | | | | | | | | | | | | | | |
| **GBW 560/4** | 5508 | 9123 | 1409 | 45 | 1.83 | 7.93 | 10.4 | 867 | 45 | 45 | 92 | **MWS 10** | 1946 | **TSW 10** | 1498 | **MW** [1] | 1579 |
| **2 speed motor, 3 Phase motor, 400 V / 3 ph. / 50 Hz, Y/△ wiring, protection to IP 54** | | | | | | | | | | | | | | | | | |
| **GBD 560/6/6** | 5522 | 7800/9000 | 705/885 | 35 | 0.51/0.80 | 0.90/1.85 | 1.90 | 867 | 60 | 60 | 80 | **RDS 4** | 1316 | **TSD 3,0** | 1502 | **MD** | 5849 |
| **GBD 560/4/4** | 5521 | 11500/13000 | 1110/1350 | 44 | 1.70/2.60 | 2.80/4.80 | 4.90 | 867 | 55 | 45 | 90 | **RDS 7** | 1578 | **TSD 7,0** | 1504 | **MD** | 5849 |
| **2 speed motor, 3 Phase motor, 400 V / 3 ph. / 50 Hz, Y/△ wiring, protection to IP 54** | | | | | | | | | | | | | | | | | |
| **GBD 560/4/4 T120** | 5778 | 11520/12300 | 1250/1400 | 48 | 1.85/2.50 | 3.20/6.80 | 6.80 | 520 | 120 | 120 | 105 | **RDS 7** | 1578 | **TSD 7,0** | 1504 | **MD** | 5849 |

1) incl. operation switch

## GBD 560/4/4

| Frequency | | Hz | Total | 125 | 250 | 500 | 1k | 2k | 4k | 8k |
|---|---|---|---|---|---|---|---|---|---|---|
| $L_{WA}$ | Case breakout | dB(A) | 64 | 64 | 64 | 48 | 50 | 46 | 43 | 37 |
| $L_{WA}$ | Intake | dB(A) | 77 | 57 | 66 | 69 | 74 | 70 | 64 | 55 |
| $L_{WA}$ | Exhaust | dB(A) | 81 | 62 | 74 | 75 | 75 | 74 | 70 | 61 |





ACOUSTICA™

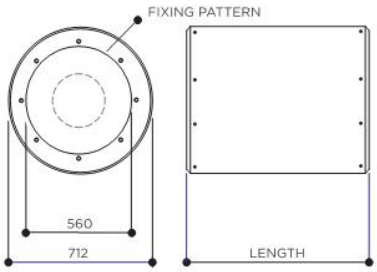
ACOUSTICA MANUFACTURING LTD
01206 852 389 info@acoustica.co acoustica.co

**CP03-C-0560**

## 560 DIA FAN MOUNTED SILENCER

Available in two standard lengths C Series Silencers have excellent attenuation properties, achieved with sound absorbing infill retained in the attenuator casing by a perforated liner. The central pod (code P) is an option to increase the insertion loss, however it will add resistance.

- Fits directly onto 560mm diameter fans
- Standard lengths 560mm (1D) & 1120mm (2D)
- Use up to 70°C (standard construction)
- Systems up to 1000 Pascals
- Special lengths on request




### INSERTION LOSS (dB) - CENTRE BAND FREQUENCY

| PRODUCT CODE | 63 Hz | 125 Hz | 250 Hz | 500 Hz | 1000 Hz | 2000 Hz | 4000 Hz | 8000 Hz |
|---|---|---|---|---|---|---|---|---|
| CP03-C*-0560-1D | 2 | 4 | 7 | 14 | 14 | 9 | 9 | 7 |
| CP03-C*-0560-2D | 3 | 6 | 10 | 19 | 20 | 14 | 12 | 10 |
| CP03-C*P-0560-1D | 3 | 7 | 9 | 18 | 24 | 24 | 20 | 15 |
| CP03-C*P-0560-2D | 4 | 9 | 17 | 27 | 29 | 28 | 23 | 23 |

Insertion loss data is derived from continual testing to BS4718 and other standards in independent UKAS certified laboratories, which includes where appropriate, re-generated or self noise testing in both forward and reverse flow conditions. If you request system analysis from our technicians all predictions will be assessed using the relevant certified insertion loss data together with relevant dynamic corrections.

### DIMENSIONAL DATA

| CODE | LENGTH | FIXING PATTERN | MASS |
|---|---|---|---|
| CP03-CA-0560-1D | 560mm | 12 x M10-620 PCD | 22 Kg |
| CP03-CA-0560-2D | 1120mm | 12 x M10-620 PCD | 48 Kg |
| CP03-CAP-0560-1D | 560mm | 12 x M10-620 PCD | 26 Kg |
| CP03-CAP-0560-2D | 1120mm | 12 x M10-620 PCD | 57 Kg |
| CP03-CB-0560-1D | 560mm | 16 x M10-605 PCD | 22 Kg |
| CP03-CB-0560-2D | 1120mm | 16 x M10-605 PCD | 48 Kg |
| CP03-CBP-0560-1D | 560mm | 16 x M10-605 PCD | 26 Kg |
| CP03-CBP-0560-2D | 1120mm | 16 x M10-605 PCD | 57 Kg |