

Northwood and Pinner Cottage Hospital, Pinner Road, HA6 1DE Drainage Strategy

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1 Site Location and Setting

The proposed development site is centred at approximate National Grid Reference (510127, 190706) and comprises of the Northwood Health Centre and the former Northwood and Pinner Cottage Hospital.

The proposed areas for re-development total approximately 7413m² with 1473 m² of Health Care floor space and 5949m². The development area is currently 61% impermeable.

The topographical site survey carried out by Alan Rhodes Associates in July 2017. The survey indicates ground levels fall in a south-westerly direction and existing levels range from The survey indicates ground levels fall in a south-westerly direction and existing levels range from 71m AOD at Pinner Road to 75m AOD in the north-east corner of the site.

The British Geological Survey (BGS) geological map for the area shows that the site's solid geology is 'London Clay Formation' -Clay, silt and sand. There are no records of superficial deposits. The BGS archive contains one record of a borehole sunk in the general vicinity of the Site. The borehole is located approximately 50m east of the site boundary and is identified by the BGS as TQ19SW40. The borehole proves approximately 0.2 m of made ground overlying the London Clay Formation to a depth of approximately 12 m below ground level (bgl). The Lambeth Group is present beneath the London Clay to a depth of 27 m bgl followed by the Seaford and Newhaven Formations to a maximum proved depth (i.e. the formation was not penetrated) of 91 m bgl.

A phase 2 Geo-environmental and Geotechnical Site Investigation was carried out by RSK in August 2020 ref. 192113401 (00). This confirmed the general finding from the BGS with 0.2-1.2m of made ground overlaying 7.3m-11.6m of London Clay overlaying the Lambeth Group to 11m+.

2 Proposed Development

This redevelopment includes the demolition of the existing healthcare practice with the construction of two new 4-storey residential block and the refurbishment of the existing cottage hospital into the new Healthcare Centre. This report summarises the brief, the existing buildings and the structural framing required to achieve the proposed redevelopment.

The proposed structure for the residential blocks is as follows;

- Columns typically 200x800, located within partitions /walls
- Flat slab typically 250mm, locally thickened
- Stability cores 250mm thick
- Steel framing to form the mansard roof with a hung plant platform
- 600mm diameter piled pad foundations

The original construction from 1925 for the healthcare centre is proposed to be retained, with local repair works where required. Later additions are to be demolished with a new 2 storey wing constructed to the north east. The proposed structure for this wing is as follows;

- Load bearing masonry walls and partitions
- Steel frame with timber joisted floor
- 600mm diameter piled foundations with a movement joint between the existing and new construction

3 Surface Water Runoff Rates

The discharge from the site must not impact the flood risk of the surrounding developments both upstream and downstream of the site.

The peak runoff rate from the development to any drain, sewer or surface water body for the 1 in 1 year rainfall event and the 1 in 100 year rainfall event should be as close as reasonably practicable to the greenfield runoff rate from the development for the same rainfall event, but should never exceed the rate of discharge from the development prior to redevelopment for that event.

In addition to this, the runoff volume for the 1 in 100-year, 6 hour rainfall event must be constrained to a value as close as is reasonably practicable to the greenfield runoff volume for the same event, but should never exceed the runoff volume from the development site prior to redevelopment for that event. However, where it is not reasonably practicable to constrain the volume the runoff volume must be discharged at a rate that does not adversely affect flood risk.

As part of the Flood Risk Assessment written by PBA in December 2017 they contacted Thames Water to determine the allowable discharge rates from the site and capacity within the public surface water sewer. Thames Water's response was as follows:

"Only when it can be proven that soakage into the ground or a connection into the adjacent watercourse is not possible would we consider a restricted discharge into the public surface water sewer network.



We would encourage techniques such as green roofs and/or permeable paving that restricts surface water discharge from your site.

When redeveloping an existing site, policy 5.13 of the London Plan and Policy 3.4 of the Supplementary Planning Guidance (Sustainable Design and Construction) states that every attempt should be made to use flow attenuation and SUDS/storage to reduce the surface water discharge from the site as much as possible.

If they are consulted as part of any planning application Thames Water Planning team would ask to see why it is not practicable to attenuate the flows to Greenfield run-off rates i.e. 5 l/s hectare of the total site area or if the site is less than hectare in size, then the flows should be reduced by 95% of existing flows. Should the policy above be followed, we would envisage no capacity concerns with regards to surface water for this site."

The catchment areas for the existing site drainage layout have been taken from the Alan Rhodes topographical survey drawings and are broken down as follows:

			Area (m²)	Runoff Coefficien	Factored Area (m²)	Total (m²)	Total Factored	
	a ti	Roof	2970	0.95	2821.5			
	pr ti	Green Roof	0	0.4	0	9917	6262.95	
	Existing D'velpmm	Hardstanding	3157	0.85	2683.45	9917	9917	6262.95
L	ш <u>ъ</u>	Soft Landscaping	3790	0.2	758			
T								

3.1 Greenfield Runoff Rate Calculation

Using the ICP SUDS Rural Runoff Calculator within Microdrainage the following values have been calculated for the 0.99ha development site catchments. As the site is currently developed (brownfield) and approx. 61% impermeable an urban factor of 0.5 has been applied The results of the calculation are shown below:

ICP SUDS Mean Annual Flood

Input Return Period (years) 1 SAAR (mm) 600 Urban 0.500 Area (ha) 0.990 Soil 0.300 Region Number Region 6 Results 1/s QBAR Rural 1.5 QBAR Urban 3.9 Q1 year 3.3 Q30 years 7.3 Q100 years 8.8

In order to keep the volume of the attenuation down to a minimum a variable flow rate discharge unit (complex outfall) will be used. This means that the corresponding restriction can be applied to the 1:1yr, 1:30yr and 1:100yr rather than restricting the flow to only one of the return periods. Using only one return period could lead to potentially discharging too great a flow for the more frequent storms, or over designing the attenuation for the less frequent.

Qbar_{urban} for the site is shown to be 3.9l/s therefore. A restriction of flows from the site will be set to match the Qbar_{urban} value of 3.9l/s for the 1yr storm, 7.3l/s for the Q30 and 8.8l/s for the 1:100yr flows from the 1.0 ha proposed development site.

3.2 Climate Change

Referencing the gov.uk website we have used table 2 to set our climate change values. Table 2 peak rainfall intensity allowance in small and urban catchments (use 1961 to 1990 baseline)

Applies across all of England	Total potential change anticipated for the '2020s' (2015 to 2039)	Total potential change anticipated for the '2050s' (2040 to 2069)	Total potential change anticipated for the '2080s' (2070 to 2115)
Upper end	10%	20%	40%
Central	5%	10%	20%



The proposed development is a mix of; a residential which is considered to have a lifetime of 100 years, and a health centre, which is considered to have a lifetime of approximately 60 years. Based on the longer development lifetime of 100 years, the range of climate change allowances to be considered for the proposed development are 20% to 40%.

4 Hierarchy of Surface Water Disposal

When developing or redeveloping a site, the control and dispersion of surface water falling on the site's catchment always has to be considered. Wherever possible runoff from developments should be managed on the surface. This enables their performance to be more easily inspected and managed with pollution incidents and potential flood risk being visible. But due to the nature of some developments this is not always possible.

If surface water is to be discharged from the site Planning Practice Guidelines state "Generally, the aim should be to discharge surface runoff as high up the following hierarchy of drainage options as reasonably practicable:

- 1. Into the ground (infiltration)
- 2. To a surface water body;
- 3. To a surface water sewer, highway drain or another drainage system;
- 4. To a combined sewer."

It is recommended to manage surface water as close to the source i.e. where the rain falls. The effective of control and management of surface water runoff will need to be addressed through the application of the above drainage hierarchy

4.1 Discharge to Ground (Infiltration)

The PBA 'Phase 1 Ground Condition Assessment (Contamination and Stability)' report dated August 2017 indicates that the site is underlain by the London Clay Formation and the Lambeth Group with White Chalk located at depth (>60m bgl)

The clays underlying the site are likely to be of low permeability and therefore it is considered that the use of infiltration drainage is unlikely to be feasible at the site. This option has therefore been discounted.

4.2 Discharge to a Surface Water Body

There are no surface water bodies on site or in the vicinity. Discharge to a surface water body is not possible.

4.3 Discharge to a Surface Water Sewer

It is our intention to maintain the existing discharge regime for the surface water from the site and connect into the existing below ground gravity drainage (albeit with a restricted and attenuated discharge rate) and allow the flows to continue to outfall to the public surface water sewer. As set out in the Non-Statutory Technical Standards for Sustainable Drainage the flow rate should be a close as practically possible to matching the 1:1yr and 1:100yr greenfield runoff rate but not exceed the discharge from the previous development.

4.4 Discharge to a Combined Sewer

This option is not applicable as there are no combined sewers in the vicinity.

5 Inclusion of Sustainable Drainage Systems (SuDS)

Sustainable drainage is a departure from the traditional approach to draining sites. There are some key principles that influence the planning and design process enabling SuDS to mimic natural drainage by:

- Storing runoff and releasing it slowly (attenuation)
- Harvesting and using the rain close to where it falls
- Allowing water to soak into the ground (infiltration)
- Slowly transporting (conveying) water on the surface
- Filtering out pollutants
- Allowing sediments to settle out by controlling the flow of the water

To fall in line with the recommendations of The Flood and Water Management Act which requires that "developers are to put SUDS in place in new developments wherever practicable.", we have reviewed the main SuDS components in line with the suitability for the proposed development.

SuDS components are a physical part of the drainage system and can be categorised as follows:.



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S	GuDS Component	Description	Suitability for Development
Green Roof		A planted soil layer is constructed on the roof of a building to create a living surface. Water is stored in the soil layer and absorbed by vegetation.	Proposed for area shown on the Architect's and Landscape Architect's plans Feasible
Rainwater Harvesting		Rainwater is collected from the roof of a building or from other paved surfaces and stored in an overground or underground tank for treatment and reuse locally. Water could be used for toilet flushing and irrigation.	Not currently in design but could be used. To be considered in detailed design Potentially Feasible
Soakaway		A soakaway is designed to allow water to quickly soak into permeable layers of soil. Constructed like a dry well, an underground pit is dug filled with gravel or rubble. Water can be piped to a soakaway where it will be stored and allowed to gradually seep into the ground.	Onsite infiltration tests show the underlying strata to be not suitable for infiltration drainage. Unfeasible
Filter Strip	Canada Cana	Filter strips are grassed or planted areas that runoff is allowed to run across to promote infiltration and cleansing.	Onsite infiltration tests show the underlying strata to be not suitable for infiltration drainage. Unfeasible
Permeable Paving	XX	Paving which allows water to soak through. Can be in the form of paving blocks with gaps between solid blocks or porous paving where water filters through the block itself. Water can be stored in the sub-base beneath or allowed to infiltrate into ground below.	External areas could utilise permeable paving discharging to a tanked subbase due to lack of infiltration suitability. Feasible
Bioretention Area		A vegetated area with gravel and sand layers below designed to channel, filter and cleanse water vertically. Water can infiltrate into the ground below or drain to a perforated pipe and be conveyed elsewhere. Bioretention systems can be integrated with tree-pits or gardens.	Not currently in design but could be used. Planted areas adjacent to parking could be used. To be considered in detailed design Potentially Feasible
Swales		Swales are vegetated shallow depressions designed to convey and filter water. These can be 'wet' where water gathers above the surface, or 'dry' where water gathers in a gravel layer beneath. Can be lined or unlined to allow infiltration.	Not currently in design but could be used. To be considered in detailed design Potentially Feasible
Pond/Basin		Ponds can be used to store and treat water. 'Wet' ponds have a constant body of water and run-off is additional, while 'dry' ponds are empty during periods without rainfall. Ponds can be designed to allow infiltration into the ground or to store water for a period of time before discharge.	Not currently in design but could be used. Small pond could be located in landscaping. To be considered in detailed design Potentially Feasible



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Wetlands are shallow vegetated water bodies with a varying water level. Specially selected plant species are used to filter water. Water flows horizontally and is gradually treated before being discharged. Wetlands can be integrated with a natural or hardscape environment.

Water can be stored in tanks, gravel or plastic crates beneath the ground to provide attenuation. Not enough space on the development to warrant feature being specified.

Unfeasible

Proposed for attenuation features.

Feasible

The proposals will utilise the green roofs to the residential and health care centre as well as underground storage as calculated in section 6.

6 Design of Attenuation Storage

The below ground drainage will be designed to ensure:

- No surcharging for the 1:1yr storm
- No flooding for all storms up to and including the critical 1:30yr storm
- Any flooding experienced for all storms in excess of 1:30yr and up to and including the 1:100yr storm will need to be contained on site posing no risk to the building or affecting safe egress from site.
- The design will be checked for the impact of climate change on the 1:100yr storm

As previously mentioned, the 1:1yr storm will be restricted to 3.9l/s, 7.3l/s for the 1:30yr and 8.8l/s for the 1:100yr flows from the 1.0 ha proposed development site. Checks will be made for the additional 40% allowance for climate change.

			Area (m²)	Runoff	Factored	Total (m²)	Total	
			Area (m-)	Coefficien	Area (m²)	rotal (III-)	Factored	
ed int	Roof	f	2523	0.95	2396.85			
oposed velpmnt	Green R	Roof	373	0.4	149.2	9917	7875.6	
vel Vel	Hardstan	nding	6039	0.85	5133.15	3317	1015.0	
P.0	Soft Lands	caping	982	0.2	196.4			

The catchment areas for the proposed site drainage layout are broken down as follows:

In order to restrict the flows ensure that no flooding occurs for the 1:100yr + 40%, 596m³ of storage volume will be required. This will be stored below ground within attenuation crates or, if used, within the voided subbase of any permeable paving. Refer to Appendix A for MicroDrainage Calculations.

7 Surface Water Management Proposal

All drainage on the site will be private and not up for adoption by water authority. An operations and maintenance manual will be issued to the onsite maintenance team at the end of the construction recommending routine tasks and timeframes to ensure that the below ground drainage is maintained in an operable state.

8 Foul Water Drainage

As part of the Flood Risk Assessment written by PBA in December 2017 they contacted Thames Water to determine the allowable foul discharge rates from the site and capacity within the public foul water sewer. Thames Water's response was as follows:

"The existing foul sewer network does have sufficient capacity to accommodate the proposed foul water discharge from the proposed development."



9 Conclusions and compliance with planning policy

This drainage strategy has been written with note to the council's water cycle strategy of reduce, recycle and re-use. Given the ground conditions the reduction of the surface water into the sewer system is limited however green roofs have been utilised to reduce some of the surface water flows. The scheme does not have any rainwater harvesting and therefore no recycle or re-use of surface water has been utilised.

As set out in the 'Planning and Flood Risk' section in National Planning Policy Framework (NPPF), 'Policy SI 13 Sustainable drainage' in the London Plan (2021) and the sustainability objectives set out in the Hillingdon Local Plan (Part 1 and 2), this drainage strategy sets out SUDS systems (green roofs and attenuation tanks) that are appropriate to the ground conditions to discharge into the surface water system at greenfield run-off rates.



Appendix A Microdrainage Calculations

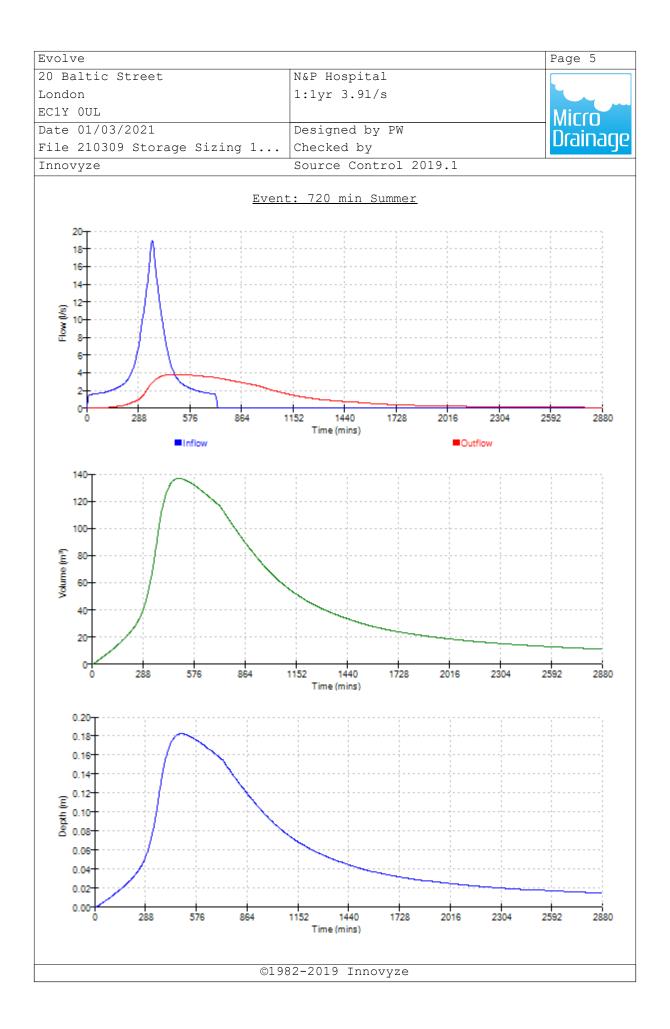
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Depre	Area ssion Storage	(m³) 373 Evaporat (mm) 5 Decay	ion (mm/day) 3 Coefficient 0.050	
	Time (mins) From: To:			nins) Area To: (ha)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0. 001368 64 0. 001120 68 0. 000917 72 0. 000751 76 0. 000615 80 0. 000503 84 0. 000412 88 0. 000337 92	68 0.000276 96 72 0.000226 100 76 0.000185 104 80 0.000152 108 84 0.000124 112 88 0.000102 116 92 0.000083 96 96 0.000068 96	100 0.000056 104 0.000046 108 0.000037 112 0.000031 116 0.000025 120 0.000021
		82-2019 Innov		

Evolve		Page 4						
20 Baltic Street	N&P Hospital							
London	1:1yr 3.91/s							
EC1Y OUL		Mirro						
Date 01/03/2021	Designed by PW	Drainage						
File 210309 Storage Sizing 1	Checked by	Diamage						
Innovyze	Source Control 2019.1	·						
In	<u>Tank or Pond Structure</u> Invert Level (m) 8.400							
Depth (m) Area (m²) Depth (m) Area (m²) D	epth (m) Area (m²) Depth (m) Area (m²) Depth	n (m) Area (m*)						
$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$		9. 600 0. 0 0. 000 0. 0						
<u>Orifi</u>	<u>ce Outflow Control</u>							

Diameter (m) 0.069 Discharge Coefficient 0.600 Invert Level (m) 8.400



Evolve					Page 1
20 Baltic Street		N&P Hospit	al		
London		1:30yr 7.3			
EC1Y OUL					Micco
Date 01/03/2021		Designed b	v PW		Micro
File 210309 Storage	Sizing 3	Checked by			Drainag
Innovyze	51111g 5 	-	trol 2019.1		
			2013.1	-	
Sumr	nary of Resu	lts for 30 y	ear Return	Period	
	-	-			
	Storm Event	Level Depth Co		tatus	
	15 min Summer 30 min Summer 10 min Summer 120 min Summer 180 min Summer 240 min Summer 360 min Summer 480 min Summer 720 min Summer 960 min Summer 240 min Summer 260 min Summer 2800 min Summer 2800 min Summer 5760 min Summer 5760 min Summer 5760 min Summer 5760 min Summer 10080 min Summer 15 min Winter 30 min Winter 120 min Winter 360 min Winter 480 min Winter	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	0 K 0 K 0 K 0 K 0 K 0 K 0 K 0 K 0 K 0 K	
	Storm Event	Rain Flooded (mm/hr) Volume (m³)	Discharge Time Volume (m (m³)		
	15 min Summer 30 min Summer 60 min Summer 120 min Summer 180 min Summer 240 min Summer 360 min Summer 360 min Summer 480 min Summer 720 min Summer 1440 min Summer 240 min Summer 570 min Summer 570 min Summer 570 min Summer 15 min Winter 30 min Winter 180 min Winter 360 min Winter 36	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$145. 2 \\ 189. 7 \\ 248. 0 \\ 296. 4 \\ 325. 3 \\ 345. 9 \\ 376. 6 \\ 399. 6 \\ 418. 0 \\ 433. 4 \\ 458. 3 \\ 493. 8 \\ 547. 3 \\ 619. 0 \\ 661. 2 \\ 687. 8 \\ 709. 0 \\ 725. 1 \\ 145. 2 \\ 189. 7 \\ 248. 0 \\ 296. 4 \\ 325. 3 \\ 345. 9 \\ 376. 6 \\ 399. 6 \\ \end{cases}$	$\begin{array}{c} 26\\ 41\\ 70\\ 126\\ 184\\ 242\\ 314\\ 376\\ 438\\ 506\\ 642\\ 914\\ 1316\\ 1704\\ 2464\\ 3176\\ 3896\\ 4600\\ 5344\\ 226\\ 40\\ 68\\ 124\\ 180\\ 236\\ 340\\ 386\\ \end{array}$	

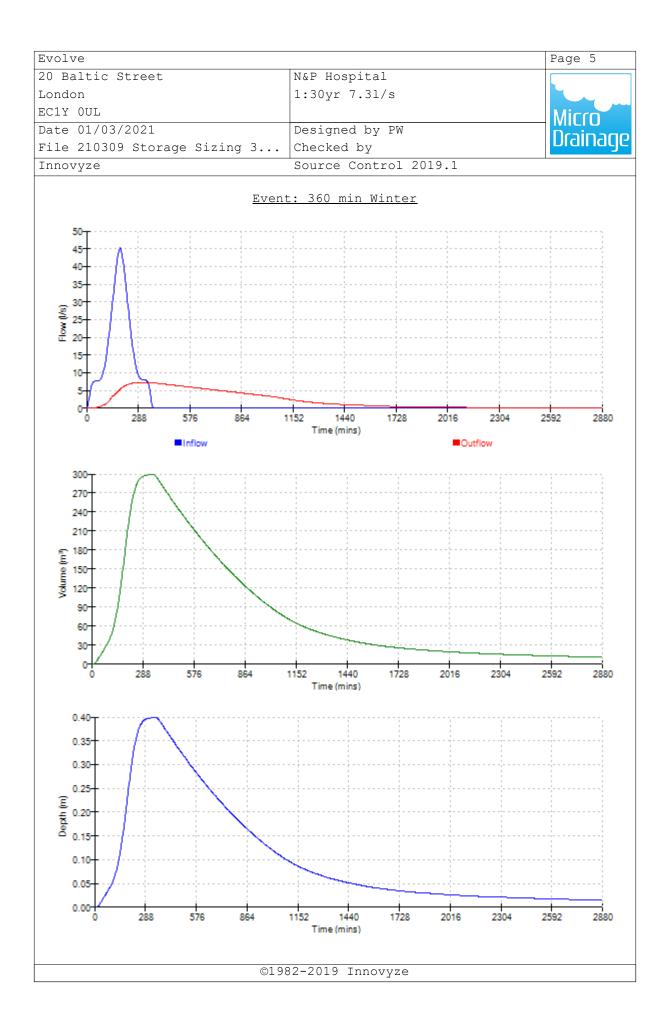
Evolve		Page 2
20 Baltic Street	N&P Hospital	
London	1:30yr 7.31/s	
EC1Y OUL		Micco
Date 01/03/2021	Designed by PW	
File 210309 Storage Sizing 3	Checked by	Drainage
Innovyze	Source Control 2019.1	
<u>Summary of Resu</u>	lts for 30 year Return Period	
2.		
Storm Event	Max Max Max Max Status Level Depth Control Volume (m) (m) (1/s) (m³)	
600 min Winter 720 min Winter	8. 793 0. 393 7. 2 294. 4 0 K 8. 787 0. 387 7. 1 290. 2 0 K	
960 min Winter 1440 min Winter	8.772 0.372 7.0 279.3 0 K	
2160 min Winter	8. 693 0. 293 6. 1 219. 7 0 K	
2880 min Winter 4320 min Winter	8 596 0 196 4 8 146 9 0 K	
5760 min Winter	8.557 0.157 4.2 118.1 0 K	
7200 min Winter 8640 min Winter	8.514 0.114 3.3 85.1 0 K	
10080 min Winter	8. 503 0. 103 3. 0 77. 5 0 K	
Storm Event	Rain Flooded Discharge Time-Peak (mm/hr) Volume Volume (mins)	
	(m ³) (m ³)	
600 min Winter 720 min Winter	5. 354 0. 0 418. 0 462 4. 628 0. 0 422 4 528	
960 min Winter	4. 628 0. 0 433. 4 538 3. 675 0. 0 458. 3 688	
1440 min Winter 2160 min Winter	2. 653 0. 0 493. 9 980 1. 913 0. 0 547. 3 1392	
2880 min Winter 4320 min Winter	1.516 0.0 577.4 1788	
5760 min Winter	0.864 0.0 661.3 3280	
7200 min Winter 8640 min Winter	0.721 0.0 688.0 3968 0.621 0.0 709.4 4664	
10080 min Winter	0. 548 0. 0 725. 9 5344	
©19	82-2019 Innovyze	

Evolve				Page 3
20 Baltic Street		N&P Hospital		
London		1:30yr 7.31/s	3	
EC1Y OUL				Micro
Date 01/03/2021		Designed by E	W	Drainage
File 210309 Storage	Sizing 3	Checked by		Drainacje
Innovyze		Source Contro	01 2019.1	
Return Pe S Time From: C	infall Model riod (years) Region Eng M5-60 (mm) Ratio R Tir To (mins) Area 1 To: (ha) F 4 0.257 Area pression Storage Time (mins) From: To: 8 32 36 0 9 36 40 4 9 36 40 44 6 6 48 52	infall Details FSR 30 Iand and Wales 20.800 Shor 0.435 Lor Yes ne Area Diagra tal Area (ha) 0.771 Fime (mins) Area rom: To: (ha) 4 8 0.257 Green Roof (m ³) 373 Evaporatio	Winter Storms) Cv (Summer) 1.0 Cv (Winter) 1.0 test Storm (mins) gest Storm (mins) 100 Climate Change % <u>m</u> Time (mins) Area From: To: (ha) 8 12 0.257 on (mm/day) 3 Coefficient 0.050 ns) Area Time (mins) Area To: (ha) 100 0.000056 104 0.000046 108 0.000037 112 0.000031 116 0.000025
16 20 0.00304 20 24 0.00249 24 28 0.00204 28 32 0.00167	4 52 56 2 56 60	0. 000615 80 0. 000503 84 0. 000412 88 0. 000337 92	84 0.000124 112 88 0.000102 116 92 0.000083 96 0.000068	116 0.00025 120 0.000021

Evolve		Page 4						
20 Baltic Street	N&P Hospital							
London	1:30yr 7.31/s							
EC1Y OUL		Micro						
Date 01/03/2021	Designed by PW	inite o						
File 210309 Storage Sizing 3	Checked by	Drainage						
Innovyze	Source Control 2019.1							
Storage is Online Cover Level (m) 10.000 <u>Tank or Pond Structure</u> Invert Level (m) 8.400								
Depth (m) Area (m²) Depth (m) Area (m²) De	epth (m) Area (m²) Depth (m) Area (m²) Depth	n (m) Area (m²)						
0.000 750.0 2.400 0.0 0.400 750.0 2.800 0.0 0.800 750.0 3.200 0.0 0.801 0.0 3.600 0.0 1.600 0.0 4.000 0.0		0. 600 0. 0 0. 000 0. 0						

Orifice Outflow Control

Diameter (m) 0.076 Discharge Coefficient 0.600 Invert Level (m) 8.400



Evolve							Page 1	
20 Baltic Street		N&P	Hospit	al				
London		1:10)0YR +	40% CC 8	8.81/s			
EC1Y OUL							Micro	
Date 01/03/2021		Desi	lgned b	y PW			Draina	nao
File 210309 Storage	Sizing 1	Chec	cked by					IJĊ
Innovyze		Sour	cce Con	trol 201	L9.1			
0		£ 1	0.0	Deturn	Develord	(1 4 0 9)		
<u>Summary</u>	of Results	IOT I	<u>JU year</u>	Return	Perioa	(+40종)		
	Storm	Max		lax Max				
	Event	(m)	<i></i>	ntrol Volur /s) (m³)				
	15 min Summer 30 min Summer 60 min Summer 120 min Summer 180 min Summer 240 min Summer 360 min Summer 480 min Summer 480 min Summer 960 min Summer 1440 min Summer 2160 min Summer 4320 min Summer 4320 min Summer 5760 min Summer 5760 min Summer 10080 min Summer 10080 min Summer 10080 min Summer 10080 min Summer 10080 min Summer 30 min Winter 120 min Winter 180 min Winter 360 min Winter 360 min Winter 360 min Winter 360 min Winter	$\begin{array}{c} 8.896\\ 9.005\\ 9.102\\ 9.147\\ 9.169\\ 9.189\\ 9.190\\ 9.186\\ 9.182\\ 9.170\\ 9.141\\ 9.090\\ 9.040\\ 8.952\\ 8.882\\ 8.825\\ 8.778\\ 8.739\\ 8.784\\ 8.896\\ 9.005\\ 9.103\\ 9.148\\ 9.005\\ 9.103\\ 9.148\\ 9.172\\ 9.192\\ \end{array}$	0. 496 0. 605 0. 702 0. 747 0. 769 0. 789 0. 780 0. 780 0. 786 0. 782 0. 770 0. 741 0. 690 0. 640 0. 652 0. 482 0. 378 0. 378 0. 384 0. 384 0. 384 0. 384 0. 384 0. 605 0. 703 0. 742 0. 772 0. 792	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9 0 K K K 9 0 K K K K 9 0 K K K K 9 0 K K K K 9 0 K K K K 9 0 K K K K 9 0 K K K K K K K K K K K K K K K K K K K			
	Storm Event	Rain (mm/hr)	Flooded Volume (m³)	Discharge Volume (m³)	Time-Peak (mins)			
1	15 min Summer 30 min Summer 60 min Summer 120 min Summer 240 min Summer 360 min Summer 480 min Summer 480 min Summer 960 min Summer 960 min Summer 2160 min Summer 2160 min Summer 2380 min Summer 4320 min Summer 4320 min Summer 7200 min Summer 7200 min Summer 7200 min Summer 7200 min Summer 7200 min Summer 7200 min Summer 15 min Winter 30 min Winter 120 min Winter 180 min Winter 240 min Winter 240 min Winter	$\begin{array}{c} 148. \ 496\\ 96. \ 016\\ 59. \ 033\\ 35. \ 052\\ 25. \ 504\\ 20. \ 240\\ 14. \ 597\\ 11. \ 570\\ 9. \ 655\\ 8. \ 325\\ 8. \ 325\\ 2. \ 670\\ 1. \ 908\\ 1. \ 908\\ 1. \ 972\\ 148. \ 496\\ 96. \ 016\\ 59. \ 033\\ 35. \ 052\\ 25. \ 504\\ 40. \ 240\\ 14. \ 597\\ \end{array}$	$\begin{array}{c} 0. \ 0 \\ 0. \ 0 \ 0 \\ 0. \ 0 \ 0 \\ 0. \ 0 \ 0 \ 0 \\ 0 \ 0 \ 0 \ 0 \ 0 \ 0 \ 0$	$\begin{array}{c} 267.\ 6\\ 343.\ 8\\ 461.\ 6\\ 549.\ 2\\ 599.\ 7\\ 634.\ 4\\ 685.\ 6\\ 723.\ 6\\ 753.\ 4\\ 777.\ 814.\ 7\\ 814.\ 7\\ 857.\ 8\\ 972.\ 9\\ 1021.\ 6\\ 1089.\ 0\\ 1156.\ 1\\ 1198.\ 2\\ 1232.\ 1\\ 1258.\ 6\\ 267.\ 6\\ 343.\ 8\\ 461.\ 6\\ 549.\ 2\\ 599.\ 7\\ 634.\ 4\\ 685.\ 7\\ \end{array}$	$\begin{array}{c} 27\\ 42\\ 70\\ 128\\ 186\\ 246\\ 362\\ 474\\ 520\\ 580\\ 704\\ 976\\ 1388\\ 1792\\ 2592\\ 3352\\ 4104\\ 4840\\ 5552\\ 27\\ 411\\ 70\\ 126\\ 184\\ 240\\ 354\end{array}$			

Evolve			Page 2
20 Baltic Street		N&P Hospital	
London		1:100YR + 40% CC 8.81/s	
EC1Y OUL			Micco
Date 01/03/2021		Designed by PW	
File 210309 Storage	Sizing 1	Checked by	Drainage
Innovyze		Source Control 2019.1	
11110 V Y Z E		Source concror zorg.r	
Gummo ra	of Poculta	<u>for 100 year Return Period (+40</u>	2)
<u>Summary</u>	OI RESUILS	IOI 100 year keturn reriou (+40-	<u>o) _</u>
	Storm	Max Max Max Max Status	
	Event	Level Depth Control Volume	
		(m) (m) (l/s) (m³)	
	600 min Winter		
	720 min Winter 960 min Winter	9. 181 0. 781 8. 6 585. 7 0 K 9. 166 0. 766 8. 5 574. 3 0 K	
	1440 min Winter	9.124 0.724 8.3 543.2 O K	
	2160 min Winter 2880 min Winter		
	4320 min Winter	8.880 0.480 6.6 360.0 0 K	
	5760 min Winter	8, 796 0, 396 6, 0 297, 4 0 K	
	7200 min Winter 8640 min Winter	8. 733 0. 333 5. 4 249. 7 0 K 8. 684 0. 284 5. 0 212. 7 0 K	
	10080 min Winter		
	Storm	Rain Flooded Discharge Time-Peak	
	Event	Rain Flooded Discharge Time-Peak (mm/hr) Volume Volume (mins)	
		(m [*]) (m [*])	
	600 min Winter	9. 655 0. 0 753. 5 566	
	720 min Winter	8. 325 0. 0 777. 8 594	
	960 min Winter 1440 min Winter	6. 584 0. 0 814. 9 740 4. 724 0. 0 858. 2 1044	
	2160 min Winter	3, 385 0, 0 973, 0 1488	
	2880 min Winter 4320 min Winter	2. 670 0. 0 1021. 7 1908 1. 908 0. 0 1089. 2 2724	
	5760 min Winter	1, 503 0, 0 1156, 2 3512	
	7200 min Winter 8640 min Winter	1. 248 0. 0 1198.4 4256 1. 072 0. 0 1232.5 5008	
	10080 min Winter	0. 942 0. 0 1259. 4 5664	
	©19	082-2019 Innovyze	

20 Baltic Street NEP Hospital London 1:100YR + 40% CC 8.81/s ECIY 0UL Designed by FW File 210309 Storage Sizing 1 Checked by Throvyze Source Control 2019.1 Rainfall Model We fee (mm) Colspan="2">Colspan="2"Colspa=
ECIY 00L Designed by PW Checked by Micro Checked by Tinnovyze Source Control 2019.1 Designed by PW Checked by Designed by PW Checked by Designed by PW Checked by Designed by PW Checked by Tinnovyze Source Control 2019.1 Rainfall Model CV (Summer) 1.000 CV (Summer) 1.0000 CV (Summer) 1.000 CV (Summer) 1.000 CV (Summer) 1.
Date 01/03/2021 Designed by PW Checked by Mintro Checked by Innovyze Source Control 2019.1 Innovyze
Date 01/03/2021 Designed by PW Checked by File 210309 Storage Sizing 1 Decinage Innovyze Source Control 2019.1 Rainfall Model Return Period (years) Return Period (years) 100 CV (Winter) 1.000 Return Period (years) 000 MS-60 (mm) 20.800 Shortest Storm (mins) Ratio R 0.435 Longest Storm (mins) Summer Storms Yes Climate Change % +40 Time Area Diagram Total Area (ha) 0.771 Time (mins) Area From: To: (ha) 0 4 0.257 4 8 0.257 Time (mins) Area From: To: (ha) Time (mins) Area (m ⁺) 373 Evaporation (mm/day) 3 Depression Storage (mm) 5 Decay Coefficient 0.050 Time (mins) Area (ha) 0.00126 From: To: (ha) Time (mins) Area (ha) 0.00126 Time (mins) Area (ha) 0.00026 From: To: (ha) Time (mins) Area (ha) 0.00026 From: To: (ha) Time (mins) Area
The 21000 biology Starting T.t. Checked by Innovyze Source Control 2019.1 Rainfall Model Return Period (years) DO Region England and Wales W5-60 (mm) Summer Storms FSR U0 CV (Winter) 1.000 CV (Summer) 1.000 CV (Summer) 1.000 CV (Summer) 1.000 CV (Summer) 1.000 Summer Storms M5-60 (mm) Summer Storms Pation Period (years) Ration R Output Output Output Output Summer Storms FSR Ves Winter Storms Yes CV (Winter) 1.000 CV (Summer) 1.000 CV (Summer) 1.000 CV (Summer) 1.000 CV (Summer) 1.000 Summer Storms Time Area Diagram Total Area (ha) 0.771 Time (mins) Area From: To: (ha) Time (mins) Area From: To: (ha) Output From: To: (ha) Output From: To: (ha) Time (mins) Area From: To: (ha) Time (mins) Area From: To: (ha) Time (mins) Area From: To: (ha) Output From: To: (ha) Output From: To: (ha) Time (mins) Area From: To: (ha)
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

Evolve Page 4							
20 Baltic Street							
London	1:100YR + 40% CC 8.81/s						
EC1Y OUL Micco							
Date 01/03/2021 Designed by PW							
File 210309 Storage Sizing 1 Checked by							
Innovyze Source Control 2019.1							
<u>Model Details</u>							

Storage is Online Cover Level (m) 10.000

Tank or Pond Structure

Invert Level (m) 8.400

Depth (m)	Area (m²)	Depth (m)	Area (m²)	Depth (m)	Area (m²)	Depth (m)	Area (m²)	Depth (m)	Area (m²)
0. 000 0. 400 0. 800 0. 801 1. 600 2. 000	750. 0 750. 0 750. 0 0. 0 0. 0 0. 0	2. 800 3. 200 3. 600 4. 000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	5. 200 5. 600 6. 000 6. 400	0.0 0.0 0.0 0.0 0.0 0.0	7. 600 8. 000 8. 400 8. 800	0.0 0.0 0.0 0.0 0.0 0.0	9. 600 10. 000	0. 0 0. 0

Orifice Outflow Control

Diameter (m) 0.069 Discharge Coefficient 0.600 Invert Level (m) 8.400

